

# **TECHNICAL SUPPLEMENT CAR WASH SPECIAL PERMIT**

**128 PLEASANT VALLEY STREET  
METHUEN, MA 01844**

**November 6, 2023**

**Prepared for:**

**Alan Kamal  
23 Equestrian Road  
Salem NH 03079  
CAQ 418**

**SUBMITTED TO:**

**CITY OF METHUEN  
ZONING BOARD OF APPEALS  
TOWN HALL  
METHUEN, MA 01844**



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## 1.0 INTRODUCTION

### **BACKGROUND:**

Alan Kamal is hereby submitting an application to the City of Methuen, for a car wash, under Zoning By-Laws, Section V-D – Use Regulations – Special Permit in a BH Zone.

The site is situated on Pleasant Valley Street and is owned by the Alan Kamal. The lot configuration (triangular) will require property offset waivers along the front and left side lot lines.

The current submittal proposes a single bay car wash, consisting of 1,588 Square Feet in a BH-5 Zone – Business Highway.

Due to the existing wetlands on Phase III, a Notice of Intent will be filed under the Wetlands Protection Act and the City of Worcester Wetlands By-law.

### ***Supplemental Information under Section XI – Special Permits***

#### ***XI – B – 2 - Special Permit Criteria***

1. *Social, Economic, or Community needs which are to be served by the proposal* – The proposed car wash operation will be the re-development of an unoccupied site. It will be compatible with surrounding businesses.
2. *Traffic flow and safety, including parking and loading* – The site has been designed to provide internal queuing of traffic, with one way traffic flow in and out via two separate curb cuts. Although there are no requirements for parking spaces, three are provided.
3. *Adequacy of utilities and other public services* – Pleasant Valley Street is serviced by all utilities at an adequate level to supply the needs of this proposal.
4. *Neighborhood character and social structures* – A car wash is compatible with surrounding character and as a business it will fit in with the neighborhood.
5. *Impacts on the natural environment* – The proposed structure will replace the previously demolished residence, garage and shed. There are no wetlands or otherwise sensitive environment.
6. *Potential fiscal impact, including impact on City services, tax base, and employment*. Said analysis shall conform with the Rules and Regulations of the SPGA – The tax base will increase based on the proposed use and structure. It is situated in a developed area and therefore well supplied with utilities. The proposed development is consistent with the Rules and Regulations of the Zoning Board of Appeals (SPGA).
7. *Consistency with the most recent City of Methuen Master Plan* – This project is consistent with neighborhood (BH).

## **DRAINAGE CALCULATIONS**

128 Pleasant Valley Street had a single family residence, which has been torn down. Previously this lot was part of a gravel operation and as such the soils on the site do not reflect the NRCS Soils, on the upper 10 feet or so. Test pits reflect the presence of sandy/gravelly soils underlying the silt loam fill. Permeability tests were conducted in the area of the proposed infiltration, using a Guelph Permeameter, with results of upwards of 30 in/hr. The drainage calculations were completed using the Cornell Atlas and Rawls infiltration rates. A second run of the drainage calculations was run using 50% of the actual infiltration rate obtained in the field testing. To be conservative the NRCS soil characteristics were used.

The Drainage Calculations for this lot have been reviewed and the existing conditions will be held. The site was analyzed in three Design Points (E-1, E-2 & E-3), for existing conditions. Design Point #E-1 is the discharge from the front-east, Design Point #E-2 is the discharge from the front west and Design Point #E-3 represents the offsite discharge to the abutting property.

The proposed conditions have been analyzed under this submittal, reflecting the same general site conditions. Design Point #P-1 reflects the runoff to street, from the front. Design Point #P-2 corresponds to E-2 and has been re-routed to flow to the west side of the property, via a small depressed area. Design Point #P-3 corresponds to E-3 and consists of the offsite drainage, being re-routed to bypass this lot. Design Point #P-4 consists of the building and the pavement, which will be collected and routed through a sediment separator and infiltrated via a subsurface system. This analysis is based on the Cornell Atlas rates.

CAQ, has performed an hydrological analysis for the applicant of the project, for the impacted areas.

This report reviews the hydrological impacts of the proposed development. The post-construction characteristics of the property were analyzed.

This system is designed to mitigate the potential for increased stormwater flows, due to the site development.

In April, 2008, DEP adopted a new Stormwater Management Policy to address the non-point pollution discharges. The Policy prescribes specific stormwater management standards for the development of projects, including urban pollutant removal criteria for projects that may impact environmental resource areas. Compliance is achieved through the implementation of “Best Management Practices” (BMP’s) in the design.

CAQ Engineering Associates, Inc. has incorporated BMP’s in the proposed SWM for the applicant of the project. Components that have been included are:

- Sedimentation Pond – forebay
- Drainage Pond – infiltration basin

## System Performance

As demonstrated below, these components, in combination will effectively mitigate post-construction rate of runoff and pollutant loading of stormwater runoff from the site. The system is projected to:

- Exceed the minimum pollutant (TSS) removal rate of 80%.
- Attenuate peak discharges, while maintaining them within the system.
- Prevent downstream flooding.

The two, ten, twenty five and one hundred year storm events were reviewed. The tables below list the rainfall intensities used for each storm event.

**Table 1 - Intensities**

<i>Storm Event</i>	<i>24 Hour Rainfall</i>	<i>Cornell Atlas</i>
<i>2 year event</i>	<i>3.20 inches</i>	<i>3.20 inches</i>
<i>10 year event</i>	<i>4.60 inches</i>	<i>4.92 inches</i>
<i>25 year event</i>	<i>5.40 inches</i>	<i>5.99 inches</i>
<i>100 year event</i>	<i>6.60 inches</i>	<i>7.65 inches</i>

**Table 2 – Comparative Analysis**

### *Pre-construction Conditions*

**D.P. # E-1      Cornell**  
2 yr event = 0.00 cfs  
10 yr event = 0.06 cfs  
50 yr. event = 0.13 cfs  
100 yr. event = 0.26 cfs

**D.P. #E-2**  
2 yr event = 0.00 cfs  
10 yr event = 0.00 cfs  
50 yr. event = 0.01 cfs  
100 yr. event = 0.02 cfs

**D.P. #E-3**  
2 yr event = 0.09 cfs  
10 yr event = 0.67 cfs  
50 yr. event = 1.15 cfs  
100 yr. event = 1.19 cfs

### *Post-construction Conditions*

**D.P. #P-1 - Cornell**  
2 yr event = 0.00 cfs  
10 yr. event = 0.00 cfs  
50 yr. event = 0.01 cfs  
100 yr. event = 0.06 cfs

**D.P. #P-2**  
2 yr event = 0.00 cfs  
10 yr. event = 0.00 cfs  
50 yr. event = 0.01 cfs  
100 yr. event = 0.00 cfs

**D.P. #P-3**  
2 yr event = 0.11 cfs  
10 yr. event = 0.60 cfs  
50 yr. event = 1.24 cfs  
100 yr. event = 2.00 cfs



**D.P. #P-4** is the infiltration pond handling the runoff from the building roof and the pavement. The analysis is based on infiltration where the 1000 year storm is above the top of the leaching, however still below the overflow elevation of 80.25.

For the 2 yr storm the maximum elevation is 74.75 with Rawls exfiltration and 74.48 with the 50% of field testing.

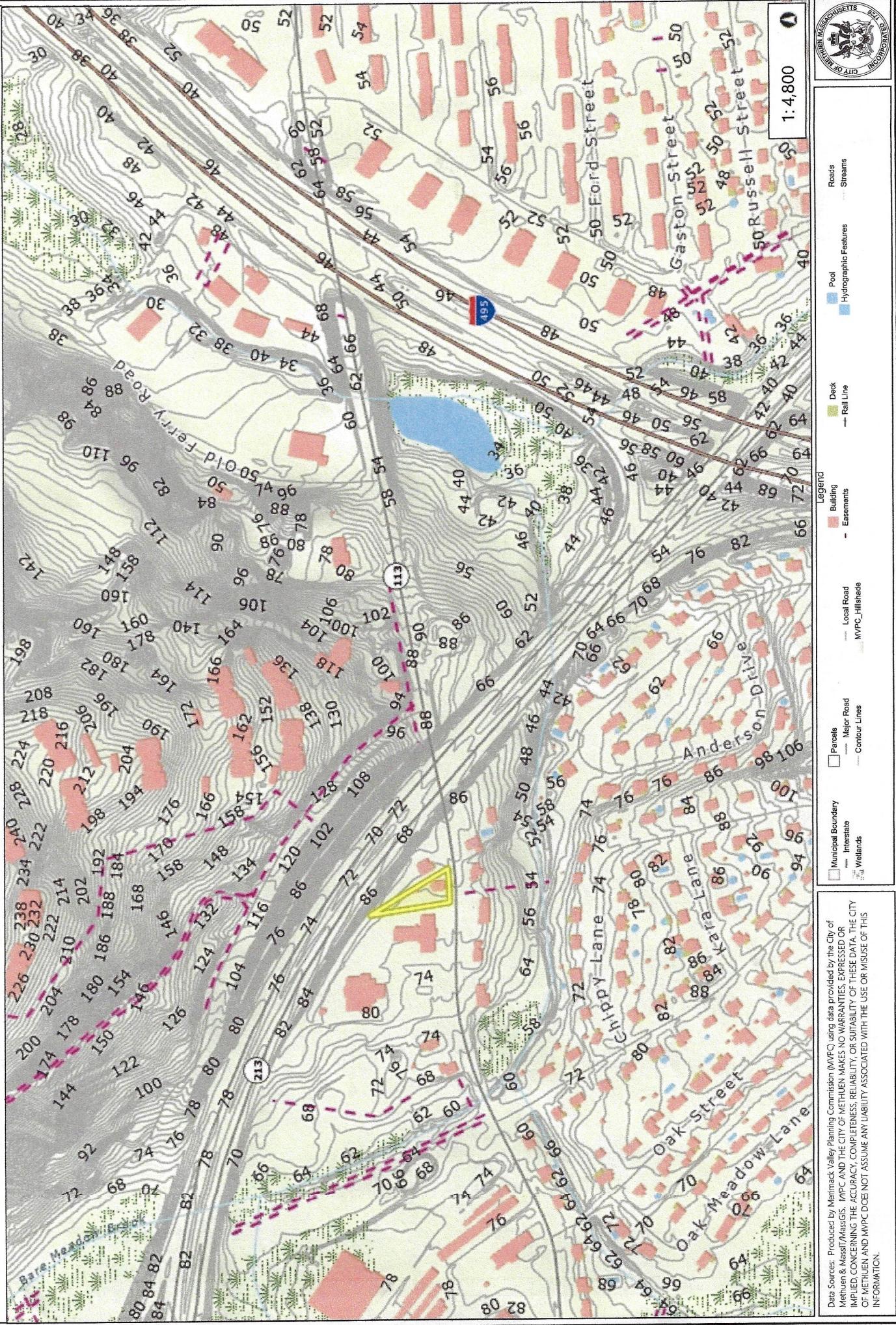
For the 10 yr storm the maximum elevation is 75.30 with Rawls exfiltration and 75.00 with the 50% of field testing

For the 50 yr storm the maximum elevation is 75.66 with Rawls exfiltration and 75.31 with the 50% of field testing

For the 100 yr storm the maximum elevation is 79.96 with Rawls exfiltration and 75.82 with the 50% of field testing

# City of Methuen

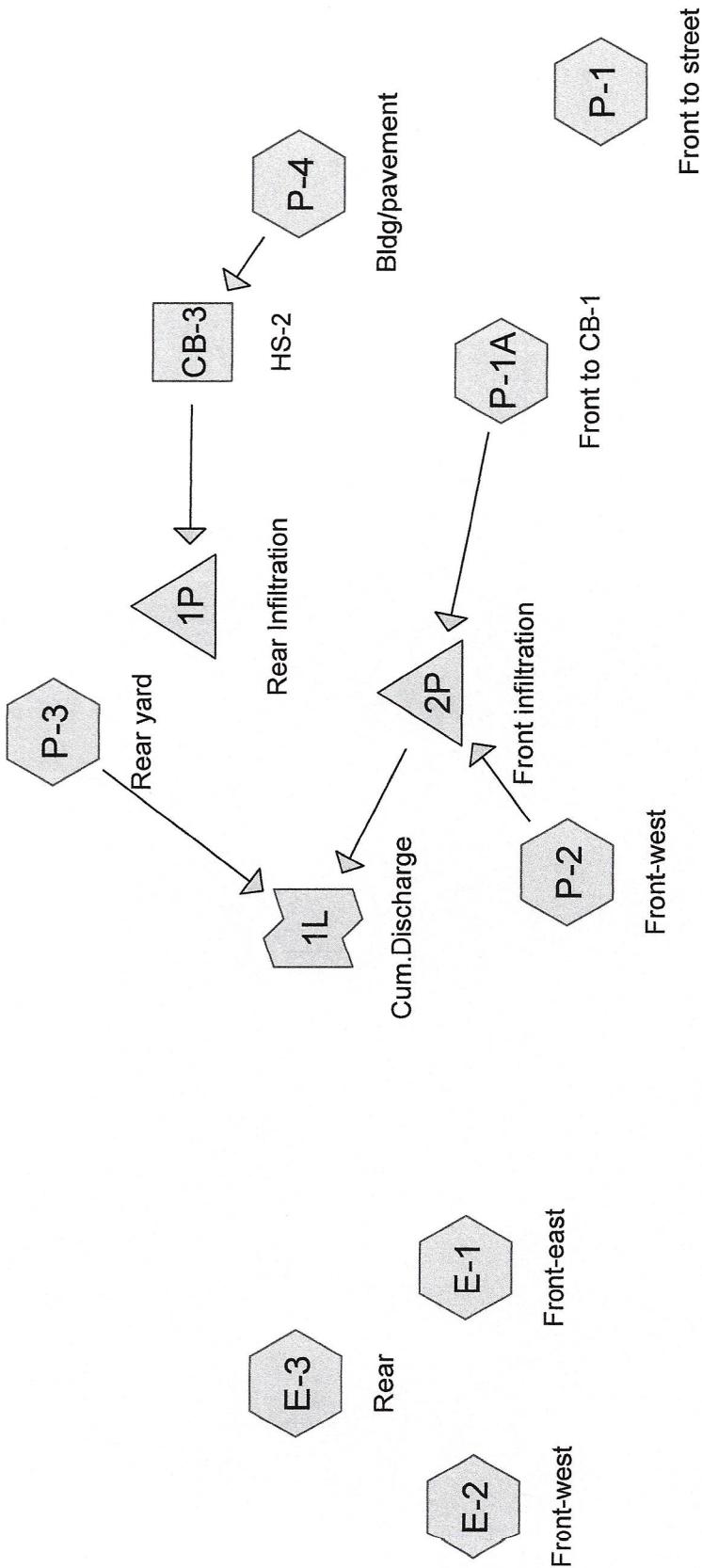
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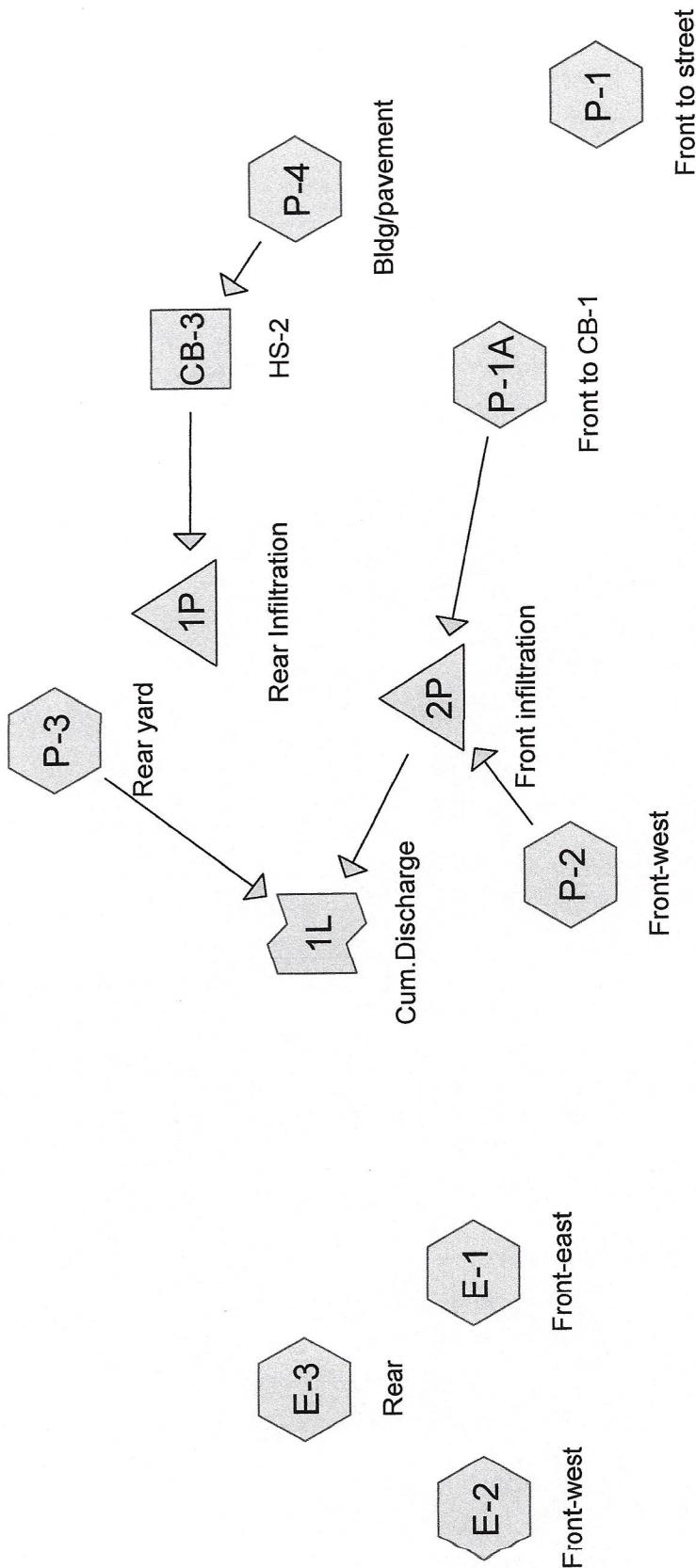
**DRAINAGE**

**PRE-DEVEVELOPMENT CONDITIONS**



**DRAINAGE**

**POST-DEVELOPMENT CONDITIONS**



**Routing Diagram for 483-Kamal-PVS**

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**483-Kamal-PVS**

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Page 1

**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
0.504	39	>75% Grass cover, Good, HSG A (E-1, E-2, E-3, P-1, P-1A, P-2, P-3, P-4)
0.375	61	>75% Grass cover, Good, HSG B (E-3, P-3, P-4)
0.143	98	Paved parking, HSG A (E-1, E-3, P-1A, P-4)
0.025	98	Paved parking, HSG B (P-4)
0.115	98	Roofs, HSG A (E-3, P-3, P-4)
<b>1.161</b>	<b>60</b>	<b>TOTAL AREA</b>

**483-Kamal-PVS**

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**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.761	HSG A	E-1, E-2, E-3, P-1, P-1A, P-2, P-3, P-4
0.399	HSG B	E-3, P-3, P-4
0.000	HSG C	
0.000	HSG D	
0.000	Other	
<b>1.161</b>		<b>TOTAL AREA</b>

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.07" Tc=6.0 min CN=48 Runoff=0.00 cfs 0.000 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>0.21" Tc=6.0 min CN=55 Runoff=0.09 cfs 0.008 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>2.20" Tc=6.0 min CN=92 Runoff=0.13 cfs 0.006 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>0.26" Tc=6.0 min CN=57 Runoff=0.11 cfs 0.008 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>2.12" Tc=0.0 min CN=91 Runoff=0.76 cfs 0.030 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/' Capacity=1.33 cfs	Avg. Flow Depth=0.27' Max Vel=6.98 fps Inflow=0.76 cfs 0.030 af Outflow=0.75 cfs 0.030 af
<b>Pond 1P: Rear Infiltration</b>	Peak Elev=74.48' Storage=183 cf Inflow=0.75 cfs 0.030 af Discarded=0.36 cfs 0.030 af Primary=0.00 cfs 0.000 af Outflow=0.36 cfs 0.030 af
<b>Pond 2P: Front infiltration</b>	Peak Elev=79.58' Storage=89 cf Inflow=0.13 cfs 0.006 af Discarded=0.04 cfs 0.006 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.006 af
<b>Link 1L: Cum.Discharge</b>	Inflow=0.11 cfs 0.008 af Primary=0.11 cfs 0.008 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.053 af Average Runoff Depth = 0.54"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.00 cfs @ 12.96 hrs, Volume= 0.000 af, Depth&gt; 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
3,138	39	>75% Grass cover, Good, HSG A
589	98	Paved parking, HSG A
3,727	48	Weighted Average
3,138		84.20% Pervious Area
589		15.80% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
752	39	>75% Grass cover, Good, HSG A
752		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 0.09 cfs @ 12.02 hrs, Volume= 0.008 af, Depth&gt; 0.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

**483-Kamal-PVS**

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Stormwater Permit  
Type II 24-hr 2yr Rainfall=3.20"

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Page 5

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.13 cfs @ 11.97 hrs, Volume= 0.006 af, Depth&gt; 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af, Depth&gt; 0.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 0.76 cfs @ 11.89 hrs, Volume= 0.030 af, Depth&gt; 2.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 2.12" for 2yr event

Inflow = 0.76 cfs @ 11.89 hrs, Volume= 0.030 af

Outflow = 0.75 cfs @ 11.89 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.98 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.11 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.27'

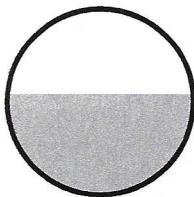
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 2.12" for 2yr event

Inflow = 0.75 cfs @ 11.89 hrs, Volume= 0.030 af

Outflow = 0.36 cfs @ 11.97 hrs, Volume= 0.030 af, Atten= 52%, Lag= 4.6 min

Discarded = 0.36 cfs @ 11.97 hrs, Volume= 0.030 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 74.48' @ 11.97 hrs Surf.Area= 945 sf Storage= 183 cf

Plug-Flow detention time= 2.8 min calculated for 0.030 af (100% of inflow)

Center-of-Mass det. time= 2.6 min ( 761.1 - 758.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.36 cfs @ 11.97 hrs HW=74.47' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.36 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 1.75" for 2yr event  
Inflow = 0.13 cfs @ 11.97 hrs, Volume= 0.006 af  
Outflow = 0.04 cfs @ 12.10 hrs, Volume= 0.006 af, Atten= 67%, Lag= 8.3 min  
Discarded = 0.04 cfs @ 12.10 hrs, Volume= 0.006 af  
Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Peak Elev= 79.58' @ 12.10 hrs Surf.Area= 226 sf Storage= 89 cf

Plug-Flow detention time= 21.1 min calculated for 0.006 af (100% of inflow)  
Center-of-Mass det. time= 20.8 min ( 780.1 - 759.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	<b>Custom Stage Data (Conic) Listed below (Recalc)</b>

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	<b>8.270 in/hr Exfiltration over Wetted area</b>
#2	Primary	79.75'	<b>25.0' long Broad-Crested Rectangular Weir</b> Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.04 cfs @ 12.10 hrs HW=79.58' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.04 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=78.50' (Free Discharge)  
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

**Summary for Link 1L: Cum.Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 0.23" for 2yr event

Inflow = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af

Primary = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.47" Tc=6.0 min CN=48 Runoff=0.06 cfs 0.003 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.14" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>0.82" Tc=6.0 min CN=55 Runoff=0.67 cfs 0.031 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.14" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>3.76" Tc=6.0 min CN=92 Runoff=0.22 cfs 0.011 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.14" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>0.94" Tc=6.0 min CN=57 Runoff=0.60 cfs 0.027 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>3.67" Tc=0.0 min CN=91 Runoff=1.26 cfs 0.053 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/' Capacity=1.33 cfs	Avg. Flow Depth=0.39' Max Vel=7.70 fps Inflow=1.26 cfs 0.053 af Outflow=1.26 cfs 0.053 af
<b>Pond 1P: Rear Infiltration</b>	Peak Elev=75.00' Storage=492 cf Inflow=1.26 cfs 0.053 af Discarded=0.40 cfs 0.053 af Primary=0.00 cfs 0.000 af Outflow=0.40 cfs 0.053 af
<b>Pond 2P: Front infiltration</b>	Peak Elev=79.77' Storage=139 cf Inflow=0.22 cfs 0.011 af Discarded=0.06 cfs 0.010 af Primary=0.13 cfs 0.001 af Outflow=0.19 cfs 0.011 af
<b>Link 1L: Cum. Discharge</b>	Inflow=0.60 cfs 0.028 af Primary=0.60 cfs 0.028 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.126 af Average Runoff Depth = 1.30"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

### Summary for Subcatchment E-1: Front-east

Runoff = 0.06 cfs @ 12.00 hrs, Volume= 0.003 af, Depth> 0.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description			
3,138	39	>75% Grass cover, Good, HSG A			
589	98	Paved parking, HSG A			
3,727	48	Weighted Average			
3,138		84.20% Pervious Area			
589		15.80% Impervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

### Summary for Subcatchment E-2: Front-west

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth> 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description			
752	39	>75% Grass cover, Good, HSG A			
752		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

### Summary for Subcatchment E-3: Rear

Runoff = 0.67 cfs @ 11.99 hrs, Volume= 0.031 af, Depth> 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth&gt; 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.22 cfs @ 11.96 hrs, Volume= 0.011 af, Depth&gt; 3.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth&gt; 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Depth&gt; 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af, Depth&gt; 3.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 3.67" for 10-yr event

Inflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af

Outflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.70 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.55 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.39'

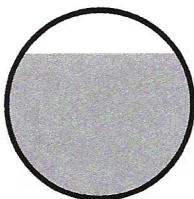
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 3.67" for 10-yr event

Inflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af

Outflow = 0.40 cfs @ 11.99 hrs, Volume= 0.053 af, Atten= 68%, Lag= 6.2 min

Discarded = 0.40 cfs @ 11.99 hrs, Volume= 0.053 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.00' @ 11.99 hrs Surf.Area= 945 sf Storage= 492 cf

Plug-Flow detention time= 6.3 min calculated for 0.053 af (100% of inflow)

Center-of-Mass det. time= 6.1 min ( 752.8 - 746.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	<b>10.00'W x 94.50'L x 2.50'H Prismatoid</b> 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	<b>18.0" Round CMP_Round 18" x 4 Inside #1</b> L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	<b>15.000 in/hr Exfiltration over Wetted area</b>
#2	Primary	79.80'	<b>18.0" Round Culvert L= 3.8' Ke= 0.900</b>

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.40 cfs @ 11.99 hrs HW=74.99' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.40 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
 ↗2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 3.03" for 10-yr event  
 Inflow = 0.22 cfs @ 11.96 hrs, Volume= 0.011 af  
 Outflow = 0.19 cfs @ 12.05 hrs, Volume= 0.011 af, Atten= 12%, Lag= 5.2 min  
 Discarded = 0.06 cfs @ 12.05 hrs, Volume= 0.010 af  
 Primary = 0.13 cfs @ 12.05 hrs, Volume= 0.001 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.77' @ 12.05 hrs Surf.Area= 310 sf Storage= 139 cf

Plug-Flow detention time= 23.4 min calculated for 0.011 af (100% of inflow)  
 Center-of-Mass det. time= 22.8 min ( 772.9 - 750.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	8.270 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.06 cfs @ 12.05 hrs HW=79.77' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.06 cfs)

**Primary OutFlow** Max=0.13 cfs @ 12.05 hrs HW=79.77' (Free Discharge)  
 ↗2=Broad-Crested Rectangular Weir (Weir Controls 0.13 cfs @ 0.23 fps)

**Summary for Link 1L: Cum.Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 0.85" for 10-yr event

Inflow = 0.60 cfs @ 12.00 hrs, Volume= 0.028 af

Primary = 0.60 cfs @ 12.00 hrs, Volume= 0.028 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.87" Tc=6.0 min CN=48 Runoff=0.13 cfs 0.006 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.36" Tc=6.0 min CN=39 Runoff=0.01 cfs 0.001 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>1.35" Tc=6.0 min CN=55 Runoff=1.15 cfs 0.051 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.36" Tc=6.0 min CN=39 Runoff=0.01 cfs 0.001 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>4.74" Tc=6.0 min CN=92 Runoff=0.27 cfs 0.014 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.36" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>1.50" Tc=6.0 min CN=57 Runoff=0.98 cfs 0.043 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>4.64" Tc=0.0 min CN=91 Runoff=1.57 cfs 0.067 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/'	Avg. Flow Depth=0.50' Max Vel=7.73 fps Inflow=1.57 cfs 0.067 af Capacity=1.33 cfs Outflow=1.35 cfs 0.067 af
<b>Pond 1P: Rear Infiltration</b> Discarded=0.42 cfs 0.067 af	Peak Elev=75.31' Storage=716 cf Inflow=1.35 cfs 0.067 af Primary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.067 af
<b>Pond 2P: Front infiltration</b> Discarded=0.06 cfs 0.012 af	Peak Elev=79.79' Storage=144 cf Inflow=0.27 cfs 0.014 af Primary=0.28 cfs 0.002 af Outflow=0.34 cfs 0.014 af
<b>Link 1L: Cum.Discharge</b>	Inflow=1.24 cfs 0.045 af Primary=1.24 cfs 0.045 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.183 af Average Runoff Depth = 1.89"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.13 cfs @ 11.99 hrs, Volume= 0.006 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description			
3,138	39	>75% Grass cover, Good, HSG A			
589	98	Paved parking, HSG A			
3,727	48	Weighted Average			
3,138		84.20% Pervious Area			
589		15.80% Impervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.01 cfs @ 12.02 hrs, Volume= 0.001 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description			
752	39	>75% Grass cover, Good, HSG A			
752		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 1.15 cfs @ 11.98 hrs, Volume= 0.051 af, Depth&gt; 1.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

**483-Kamal-PVS**

Prepared by CAQ Engineering Associates, Inc.

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Stormwater Permit  
 Type II 24-hr 50-yr Rainfall=5.99"  
 Printed 11/5/2023  
 Page 19

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.01 cfs @ 12.02 hrs, Volume= 0.001 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.27 cfs @ 11.96 hrs, Volume= 0.014 af, Depth&gt; 4.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 12.02 hrs, Volume= 0.000 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.98 cfs @ 11.98 hrs, Volume= 0.043 af, Depth&gt; 1.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 1.57 cfs @ 11.89 hrs, Volume= 0.067 af, Depth&gt; 4.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 4.64" for 50-yr event  
 Inflow = 1.57 cfs @ 11.89 hrs, Volume= 0.067 af  
 Outflow = 1.35 cfs @ 11.88 hrs, Volume= 0.067 af, Atten= 14%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.73 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.75 fps, Avg. Travel Time= 0.1 min

Peak Storage= 2 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.50'

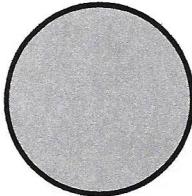
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 4.64" for 50-yr event  
 Inflow = 1.35 cfs @ 11.88 hrs, Volume= 0.067 af  
 Outflow = 0.42 cfs @ 12.01 hrs, Volume= 0.067 af, Atten= 69%, Lag= 7.8 min  
 Discarded = 0.42 cfs @ 12.01 hrs, Volume= 0.067 af  
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.31' @ 12.01 hrs Surf.Area= 945 sf Storage= 716 cf

Plug-Flow detention time= 8.9 min calculated for 0.067 af (100% of inflow)

Center-of-Mass det. time= 8.7 min ( 751.2 - 742.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.42 cfs @ 12.01 hrs HW=75.31' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.42 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
 ↗2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 3.85" for 50-yr event  
 Inflow = 0.27 cfs @ 11.96 hrs, Volume= 0.014 af  
 Outflow = 0.34 cfs @ 12.00 hrs, Volume= 0.014 af, Atten= 0%, Lag= 2.4 min  
 Discarded = 0.06 cfs @ 12.01 hrs, Volume= 0.012 af  
 Primary = 0.28 cfs @ 12.00 hrs, Volume= 0.002 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.79' @ 12.01 hrs Surf.Area= 317 sf Storage= 144 cf

Plug-Flow detention time= 22.3 min calculated for 0.014 af (99% of inflow)  
 Center-of-Mass det. time= 21.2 min ( 768.2 - 747.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	8.270 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.06 cfs @ 12.01 hrs HW=79.79' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.06 cfs)

**Primary OutFlow** Max=0.26 cfs @ 12.00 hrs HW=79.79' (Free Discharge)  
 ↗2=Broad-Crested Rectangular Weir (Weir Controls 0.26 cfs @ 0.28 fps)

**Summary for Link 1L: Cum. Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 1.39" for 50-yr event

Inflow = 1.24 cfs @ 11.99 hrs, Volume= 0.045 af

Primary = 1.24 cfs @ 11.99 hrs, Volume= 0.045 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>1.64" Tc=6.0 min CN=48 Runoff=0.26 cfs 0.012 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.02 cfs 0.001 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>2.30" Tc=6.0 min CN=55 Runoff=1.99 cfs 0.087 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.06 cfs 0.003 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>6.25" Tc=6.0 min CN=92 Runoff=0.35 cfs 0.018 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.01 cfs 0.001 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>2.50" Tc=6.0 min CN=57 Runoff=1.66 cfs 0.072 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>6.16" Tc=0.0 min CN=91 Runoff=2.04 cfs 0.089 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/'	Avg. Flow Depth=0.50' Max Vel=7.73 fps Inflow=2.04 cfs 0.089 af Capacity=1.33 cfs Outflow=1.37 cfs 0.089 af
<b>Pond 1P: Rear Infiltration</b> Discarded=0.46 cfs 0.089 af	Peak Elev=75.82' Storage=1,055 cf Inflow=1.37 cfs 0.089 af Primary=0.00 cfs 0.000 af Outflow=0.46 cfs 0.089 af
<b>Pond 2P: Front infiltration</b> Discarded=0.06 cfs 0.015 af	Peak Elev=79.80' Storage=147 cf Inflow=0.36 cfs 0.019 af Primary=0.38 cfs 0.004 af Outflow=0.44 cfs 0.019 af
<b>Link 1L: Cum.Discharge</b>	Inflow=2.00 cfs 0.076 af Primary=2.00 cfs 0.076 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.282 af Average Runoff Depth = 2.92"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.26 cfs @ 11.99 hrs, Volume= 0.012 af, Depth&gt; 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
3,138	39	>75% Grass cover, Good, HSG A
589	98	Paved parking, HSG A
3,727	48	Weighted Average
3,138		84.20% Pervious Area
589		15.80% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.02 cfs @ 12.00 hrs, Volume= 0.001 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
752	39	>75% Grass cover, Good, HSG A
752		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 1.99 cfs @ 11.98 hrs, Volume= 0.087 af, Depth&gt; 2.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.06 cfs @ 12.00 hrs, Volume= 0.003 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.35 cfs @ 11.96 hrs, Volume= 0.018 af, Depth&gt; 6.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.01 cfs @ 12.00 hrs, Volume= 0.001 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-3: Rear yard**

Runoff = 1.66 cfs @ 11.98 hrs, Volume= 0.072 af, Depth&gt; 2.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 2.04 cfs @ 11.89 hrs, Volume= 0.089 af, Depth&gt; 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

### Summary for Reach CB-3: HS-2

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 6.16" for 100-yr event  
 Inflow = 2.04 cfs @ 11.89 hrs, Volume= 0.089 af  
 Outflow = 1.37 cfs @ 12.00 hrs, Volume= 0.089 af, Atten= 33%, Lag= 6.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.73 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 3.01 fps, Avg. Travel Time= 0.0 min

Peak Storage= 2 cf @ 11.85 hrs

Average Depth at Peak Storage= 0.50'

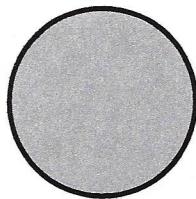
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'



### Summary for Pond 1P: Rear Infiltration

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 6.16" for 100-yr event  
 Inflow = 1.37 cfs @ 12.00 hrs, Volume= 0.089 af  
 Outflow = 0.46 cfs @ 12.06 hrs, Volume= 0.089 af, Atten= 66%, Lag= 3.4 min  
 Discarded = 0.46 cfs @ 12.06 hrs, Volume= 0.089 af  
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.82' @ 12.06 hrs Surf.Area= 945 sf Storage= 1,055 cf

Plug-Flow detention time= 12.9 min calculated for 0.089 af (100% of inflow)

Center-of-Mass det. time= 12.7 min ( 750.9 - 738.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.46 cfs @ 12.06 hrs HW=75.81' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.46 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 5.16" for 100-yr event  
 Inflow = 0.36 cfs @ 11.96 hrs, Volume= 0.019 af  
 Outflow = 0.44 cfs @ 11.96 hrs, Volume= 0.019 af, Atten= 0%, Lag= 0.0 min  
 Discarded = 0.06 cfs @ 11.96 hrs, Volume= 0.015 af  
 Primary = 0.38 cfs @ 11.96 hrs, Volume= 0.004 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.80' @ 11.96 hrs Surf.Area= 321 sf Storage= 147 cf

Plug-Flow detention time= 21.2 min calculated for 0.018 af (99% of inflow)  
 Center-of-Mass det. time= 19.5 min ( 763.5 - 743.9 )

Volume	Invert	Avail.Storage	Storage Description	
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	8.270 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.06 cfs @ 11.96 hrs HW=79.79' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.06 cfs)

**Primary OutFlow** Max=0.33 cfs @ 11.96 hrs HW=79.79' (Free Discharge)  
2=Broad-Crested Rectangular Weir (Weir Controls 0.33 cfs @ 0.31 fps)

**Summary for Link 1L: Cum.Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 2.34" for 100-yr event  
Inflow = 2.00 cfs @ 11.97 hrs, Volume= 0.076 af  
Primary = 2.00 cfs @ 11.97 hrs, Volume= 0.076 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**Area Listing (all nodes)**

Area (acres)	CN	Description (subcatchment-numbers)
0.504	39	>75% Grass cover, Good, HSG A (E-1, E-2, E-3, P-1, P-1A, P-2, P-3, P-4)
0.375	61	>75% Grass cover, Good, HSG B (E-3, P-3, P-4)
0.143	98	Paved parking, HSG A (E-1, E-3, P-1A, P-4)
0.025	98	Paved parking, HSG B (P-4)
0.115	98	Roofs, HSG A (E-3, P-3, P-4)
<b>1.161</b>	<b>60</b>	<b>TOTAL AREA</b>

**Soil Listing (all nodes)**

Area (acres)	Soil Group	Subcatchment Numbers
0.761	HSG A	E-1, E-2, E-3, P-1, P-1A, P-2, P-3, P-4
0.399	HSG B	E-3, P-3, P-4
0.000	HSG C	
0.000	HSG D	
0.000	Other	
<b>1.161</b>		<b>TOTAL AREA</b>

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.07" Tc=6.0 min CN=48 Runoff=0.00 cfs 0.000 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>0.21" Tc=6.0 min CN=55 Runoff=0.09 cfs 0.008 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>2.20" Tc=6.0 min CN=92 Runoff=0.13 cfs 0.006 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth=0.00" Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>0.26" Tc=6.0 min CN=57 Runoff=0.11 cfs 0.008 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>2.12" Tc=0.0 min CN=91 Runoff=0.76 cfs 0.030 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/' Capacity=1.33 cfs Outflow=0.75 cfs 0.030 af	Avg. Flow Depth=0.27' Max Vel=6.98 fps Inflow=0.76 cfs 0.030 af
<b>Pond 1P: Rear Infiltration</b>	Peak Elev=74.48' Storage=183 cf Inflow=0.75 cfs 0.030 af Discarded=0.36 cfs 0.030 af Primary=0.00 cfs 0.000 af Outflow=0.36 cfs 0.030 af
<b>Pond 2P: Front infiltration</b>	Peak Elev=79.48' Storage=67 cf Inflow=0.13 cfs 0.006 af Discarded=0.07 cfs 0.006 af Primary=0.00 cfs 0.000 af Outflow=0.07 cfs 0.006 af
<b>Link 1L: Cum.Discharge</b>	Inflow=0.11 cfs 0.008 af Primary=0.11 cfs 0.008 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.053 af Average Runoff Depth = 0.54"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.00 cfs @ 12.96 hrs, Volume= 0.000 af, Depth&gt; 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
3,138	39	>75% Grass cover, Good, HSG A
589	98	Paved parking, HSG A
3,727	48	Weighted Average
3,138		84.20% Pervious Area
589		15.80% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
752	39	>75% Grass cover, Good, HSG A
752		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 0.09 cfs @ 12.02 hrs, Volume= 0.008 af, Depth&gt; 0.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

**483-Kamal-PVS**

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Permeability of 15.0 in/hr  
Type II 24-hr 2yr Rainfall=3.20"

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Page 5

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.13 cfs @ 11.97 hrs, Volume= 0.006 af, Depth&gt; 2.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

**483-Kamal-PVS**

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Permeability of 15.0 in/hr  
Type II 24-hr 2yr Rainfall=3.20"

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Page 6

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af, Depth&gt; 0.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 0.76 cfs @ 11.89 hrs, Volume= 0.030 af, Depth&gt; 2.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 2yr Rainfall=3.20"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**483-Kamal-PVS**

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Permeability of 15.0 in/hr  
Type II 24-hr 2yr Rainfall=3.20"

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Page 7

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 2.12" for 2yr event  
 Inflow = 0.76 cfs @ 11.89 hrs, Volume= 0.030 af  
 Outflow = 0.75 cfs @ 11.89 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.98 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.11 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.27'

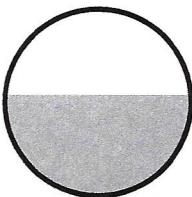
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 2.12" for 2yr event  
 Inflow = 0.75 cfs @ 11.89 hrs, Volume= 0.030 af  
 Outflow = 0.36 cfs @ 11.97 hrs, Volume= 0.030 af, Atten= 52%, Lag= 4.6 min  
 Discarded = 0.36 cfs @ 11.97 hrs, Volume= 0.030 af  
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 74.48' @ 11.97 hrs Surf.Area= 945 sf Storage= 183 cf

Plug-Flow detention time= 2.8 min calculated for 0.030 af (100% of inflow)

Center-of-Mass det. time= 2.6 min ( 761.1 - 758.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
		1,342 cf	Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.36 cfs @ 11.97 hrs HW=74.47' (Free Discharge)  
↑1=Exfiltration (Exfiltration Controls 0.36 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
↑2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 1.75" for 2yr event  
 Inflow = 0.13 cfs @ 11.97 hrs, Volume= 0.006 af  
 Outflow = 0.07 cfs @ 12.07 hrs, Volume= 0.006 af, Atten= 51%, Lag= 6.2 min  
 Discarded = 0.07 cfs @ 12.07 hrs, Volume= 0.006 af  
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.48' @ 12.07 hrs Surf.Area= 185 sf Storage= 67 cf

Plug-Flow detention time= 9.5 min calculated for 0.006 af (100% of inflow)  
 Center-of-Mass det. time= 9.4 min ( 768.7 - 759.3 )

Volume	Invert	Avail.Storage	Storage Description	
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.06 cfs @ 12.07 hrs HW=79.47' (Free Discharge)  
↑1=Exfiltration (Exfiltration Controls 0.06 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=78.50' (Free Discharge)  
↑2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

**Summary for Link 1L: Cum. Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 0.23" for 2yr event

Inflow = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af

Primary = 0.11 cfs @ 12.01 hrs, Volume= 0.008 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment E-1: Front-east**Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.47"  
Tc=6.0 min CN=48 Runoff=0.06 cfs 0.003 af**Subcatchment E-2: Front-west**Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.14"  
Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af**Subcatchment E-3: Rear**Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>0.82"  
Tc=6.0 min CN=55 Runoff=0.67 cfs 0.031 af**Subcatchment P-1: Front to street**Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.14"  
Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af**Subcatchment P-1A: Front to CB-1**Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>3.76"  
Tc=6.0 min CN=92 Runoff=0.22 cfs 0.011 af**Subcatchment P-2: Front-west**Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.14"  
Tc=6.0 min CN=39 Runoff=0.00 cfs 0.000 af**Subcatchment P-3: Rear yard**Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>0.94"  
Tc=6.0 min CN=57 Runoff=0.60 cfs 0.027 af**Subcatchment P-4: Bldg/pavement**Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>3.67"  
Tc=0.0 min CN=91 Runoff=1.26 cfs 0.053 af**Reach CB-3: HS-2**

Avg. Flow Depth=0.39' Max Vel=7.70 fps Inflow=1.26 cfs 0.053 af

6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/' Capacity=1.33 cfs Outflow=1.26 cfs 0.053 af

**Pond 1P: Rear Infiltration**

Peak Elev=75.00' Storage=492 cf Inflow=1.26 cfs 0.053 af

Discarded=0.40 cfs 0.053 af Primary=0.00 cfs 0.000 af Outflow=0.40 cfs 0.053 af

**Pond 2P: Front infiltration**

Peak Elev=79.71' Storage=121 cf Inflow=0.22 cfs 0.011 af

Discarded=0.10 cfs 0.011 af Primary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.011 af

**Link 1L: Cum. Discharge**

Inflow=0.60 cfs 0.027 af

Primary=0.60 cfs 0.027 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.126 af Average Runoff Depth = 1.30"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.06 cfs @ 12.00 hrs, Volume= 0.003 af, Depth&gt; 0.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description			
3,138	39	>75% Grass cover, Good, HSG A			
589	98	Paved parking, HSG A			
3,727	48	Weighted Average			
3,138		84.20% Pervious Area			
589		15.80% Impervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth&gt; 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description			
752	39	>75% Grass cover, Good, HSG A			
752		100.00% Pervious Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 0.67 cfs @ 11.99 hrs, Volume= 0.031 af, Depth&gt; 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

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Permeability of 15.0 in/hr  
Type II 24-hr 10-yr Rainfall=4.92"

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Page 12

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth&gt; 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.22 cfs @ 11.96 hrs, Volume= 0.011 af, Depth&gt; 3.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 12.39 hrs, Volume= 0.000 af, Depth&gt; 0.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

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Permeability of 15.0 in/hr  
Type II 24-hr 10-yr Rainfall=4.92"

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Page 13

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Depth&gt; 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af, Depth&gt; 3.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 10-yr Rainfall=4.92"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 3.67" for 10-yr event

Inflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af

Outflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.70 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.55 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.39'

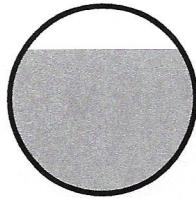
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 3.67" for 10-yr event

Inflow = 1.26 cfs @ 11.89 hrs, Volume= 0.053 af

Outflow = 0.40 cfs @ 11.99 hrs, Volume= 0.053 af, Atten= 68%, Lag= 6.2 min

Discarded = 0.40 cfs @ 11.99 hrs, Volume= 0.053 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.00' @ 11.99 hrs Surf.Area= 945 sf Storage= 492 cf

Plug-Flow detention time= 6.3 min calculated for 0.053 af (100% of inflow)

Center-of-Mass det. time= 6.1 min ( 752.8 - 746.8 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	<b>10.00'W x 94.50'L x 2.50'H Prismatoid</b> 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	<b>18.0" Round CMP_Round 18" x 4 Inside #1</b> L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	<b>15.000 in/hr Exfiltration over Wetted area</b>
#2	Primary	79.80'	<b>18.0" Round Culvert L= 3.8' Ke= 0.900</b>

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.40 cfs @ 11.99 hrs HW=74.99' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.40 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 3.03" for 10-yr event  
Inflow = 0.22 cfs @ 11.96 hrs, Volume= 0.011 af  
Outflow = 0.10 cfs @ 12.07 hrs, Volume= 0.011 af, Atten= 55%, Lag= 6.6 min  
Discarded = 0.10 cfs @ 12.07 hrs, Volume= 0.011 af  
Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Peak Elev= 79.71' @ 12.07 hrs Surf.Area= 281 sf Storage= 121 cf

Plug-Flow detention time= 11.7 min calculated for 0.011 af (100% of inflow)  
Center-of-Mass det. time= 11.5 min ( 761.6 - 750.1 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.10 cfs @ 12.07 hrs HW=79.71' (Free Discharge)  
1=Exfiltration (Exfiltration Controls 0.10 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=78.50' (Free Discharge)  
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Permeability of 15.0 in/hr  
Type II 24-hr 10-yr Rainfall=4.92"

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Page 16

### **Summary for Link 1L: Cum.Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 0.83" for 10-yr event

Inflow = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af

Primary = 0.60 cfs @ 11.99 hrs, Volume= 0.027 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>0.87" $T_c=6.0 \text{ min } CN=48$ Runoff=0.13 cfs 0.006 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.36" $T_c=6.0 \text{ min } CN=39$ Runoff=0.01 cfs 0.001 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>1.35" $T_c=6.0 \text{ min } CN=55$ Runoff=1.15 cfs 0.051 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.36" $T_c=6.0 \text{ min } CN=39$ Runoff=0.01 cfs 0.001 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>4.74" $T_c=6.0 \text{ min } CN=92$ Runoff=0.27 cfs 0.014 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.36" $T_c=6.0 \text{ min } CN=39$ Runoff=0.00 cfs 0.000 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>1.50" $T_c=6.0 \text{ min } CN=57$ Runoff=0.98 cfs 0.043 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>4.64" $T_c=0.0 \text{ min } CN=91$ Runoff=1.57 cfs 0.067 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe $n=0.010$ $L=9.0'$ $S=0.0333 '/'$ Capacity=1.33 cfs	Avg. Flow Depth=0.50' Max Vel=7.73 fps Inflow=1.57 cfs 0.067 af Outflow=1.35 cfs 0.067 af
<b>Pond 1P: Rear Infiltration</b>	Peak Elev=75.31' Storage=716 cf Inflow=1.35 cfs 0.067 af Discarded=0.42 cfs 0.067 af Primary=0.00 cfs 0.000 af Outflow=0.42 cfs 0.067 af
<b>Pond 2P: Front infiltration</b>	Peak Elev=79.77' Storage=139 cf Inflow=0.27 cfs 0.014 af Discarded=0.11 cfs 0.013 af Primary=0.12 cfs 0.001 af Outflow=0.23 cfs 0.014 af
<b>Link 1L: Cum.Discharge</b>	Inflow=1.00 cfs 0.044 af Primary=1.00 cfs 0.044 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.183 af Average Runoff Depth = 1.89"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.13 cfs @ 11.99 hrs, Volume= 0.006 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
3,138	39	>75% Grass cover, Good, HSG A
589	98	Paved parking, HSG A
3,727	48	Weighted Average
3,138		84.20% Pervious Area
589		15.80% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.01 cfs @ 12.02 hrs, Volume= 0.001 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
752	39	>75% Grass cover, Good, HSG A
752		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 1.15 cfs @ 11.98 hrs, Volume= 0.051 af, Depth&gt; 1.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

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Permeability of 15.0 in/hr  
Type II 24-hr 50-yr Rainfall=5.99"

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Page 19

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.01 cfs @ 12.02 hrs, Volume= 0.001 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.27 cfs @ 11.96 hrs, Volume= 0.014 af, Depth&gt; 4.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.00 cfs @ 12.02 hrs, Volume= 0.000 af, Depth&gt; 0.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

**483-Kamal-PVS**

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Permeability of 15.0 in/hr  
Type II 24-hr 50-yr Rainfall=5.99"

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Page 20

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-3: Rear yard**

Runoff = 0.98 cfs @ 11.98 hrs, Volume= 0.043 af, Depth&gt; 1.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-4: Bldg/pavement**

Runoff = 1.57 cfs @ 11.89 hrs, Volume= 0.067 af, Depth&gt; 4.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 50-yr Rainfall=5.99"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 4.64" for 50-yr event

Inflow = 1.57 cfs @ 11.89 hrs, Volume= 0.067 af

Outflow = 1.35 cfs @ 11.88 hrs, Volume= 0.067 af, Atten= 14%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.73 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 2.75 fps, Avg. Travel Time= 0.1 min

Peak Storage= 2 cf @ 11.89 hrs

Average Depth at Peak Storage= 0.50'

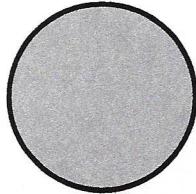
Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe

n= 0.010 PVC, smooth interior

Length= 9.0' Slope= 0.0333 '/

Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth &gt; 4.64" for 50-yr event

Inflow = 1.35 cfs @ 11.88 hrs, Volume= 0.067 af

Outflow = 0.42 cfs @ 12.01 hrs, Volume= 0.067 af, Atten= 69%, Lag= 7.8 min

Discarded = 0.42 cfs @ 12.01 hrs, Volume= 0.067 af

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 75.31' @ 12.01 hrs Surf.Area= 945 sf Storage= 716 cf

Plug-Flow detention time= 8.9 min calculated for 0.067 af (100% of inflow)

Center-of-Mass det. time= 8.7 min ( 751.2 - 742.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.42 cfs @ 12.01 hrs HW=75.31' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.42 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
 ↗2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 3.85" for 50-yr event  
 Inflow = 0.27 cfs @ 11.96 hrs, Volume= 0.014 af  
 Outflow = 0.23 cfs @ 12.05 hrs, Volume= 0.014 af, Atten= 15%, Lag= 4.9 min  
 Discarded = 0.11 cfs @ 12.04 hrs, Volume= 0.013 af  
 Primary = 0.12 cfs @ 12.05 hrs, Volume= 0.001 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.77' @ 12.04 hrs Surf.Area= 309 sf Storage= 139 cf

Plug-Flow detention time= 11.8 min calculated for 0.014 af (100% of inflow)  
 Center-of-Mass det. time= 11.6 min ( 758.6 - 747.0 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.11 cfs @ 12.04 hrs HW=79.77' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.11 cfs)

**Primary OutFlow** Max=0.11 cfs @ 12.05 hrs HW=79.77' (Free Discharge)  
 ↗2=Broad-Crested Rectangular Weir (Weir Controls 0.11 cfs @ 0.22 fps)

**Summary for Link 1L: Cum. Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 1.35" for 50-yr event

Inflow = 1.00 cfs @ 11.99 hrs, Volume= 0.044 af

Primary = 1.00 cfs @ 11.99 hrs, Volume= 0.044 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

<b>Subcatchment E-1: Front-east</b>	Runoff Area=3,727 sf 15.80% Impervious Runoff Depth>1.64" Tc=6.0 min CN=48 Runoff=0.26 cfs 0.012 af
<b>Subcatchment E-2: Front-west</b>	Runoff Area=752 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.02 cfs 0.001 af
<b>Subcatchment E-3: Rear</b>	Runoff Area=19,708 sf 10.57% Impervious Runoff Depth>2.30" Tc=6.0 min CN=55 Runoff=1.99 cfs 0.087 af
<b>Subcatchment P-1: Front to street</b>	Runoff Area=1,828 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.06 cfs 0.003 af
<b>Subcatchment P-1A: Front to CB-1</b>	Runoff Area=1,500 sf 89.47% Impervious Runoff Depth>6.25" Tc=6.0 min CN=92 Runoff=0.35 cfs 0.018 af
<b>Subcatchment P-2: Front-west</b>	Runoff Area=382 sf 0.00% Impervious Runoff Depth>0.87" Tc=6.0 min CN=39 Runoff=0.01 cfs 0.001 af
<b>Subcatchment P-3: Rear yard</b>	Runoff Area=15,129 sf 11.32% Impervious Runoff Depth>2.50" Tc=6.0 min CN=57 Runoff=1.66 cfs 0.072 af
<b>Subcatchment P-4: Bldg/pavement</b>	Runoff Area=7,528 sf 87.30% Impervious Runoff Depth>6.16" Tc=0.0 min CN=91 Runoff=2.04 cfs 0.089 af
<b>Reach CB-3: HS-2</b> 6.0" Round Pipe n=0.010 L=9.0' S=0.0333 '/'	Avg. Flow Depth=0.50' Max Vel=7.73 fps Inflow=2.04 cfs 0.089 af Capacity=1.33 cfs Outflow=1.37 cfs 0.089 af
<b>Pond 1P: Rear Infiltration</b>	Peak Elev=75.82' Storage=1,055 cf Inflow=1.37 cfs 0.089 af Discarded=0.46 cfs 0.089 af Primary=0.00 cfs 0.000 af Outflow=0.46 cfs 0.089 af
<b>Pond 2P: Front infiltration</b>	Peak Elev=79.79' Storage=144 cf Inflow=0.36 cfs 0.019 af Discarded=0.11 cfs 0.016 af Primary=0.30 cfs 0.002 af Outflow=0.41 cfs 0.019 af
<b>Link 1L: Cum.Discharge</b>	Inflow=1.94 cfs 0.075 af Primary=1.94 cfs 0.075 af

**Total Runoff Area = 1.161 ac Runoff Volume = 0.282 af Average Runoff Depth = 2.92"**  
**75.67% Pervious = 0.878 ac 24.33% Impervious = 0.282 ac**

**Summary for Subcatchment E-1: Front-east**

Runoff = 0.26 cfs @ 11.99 hrs, Volume= 0.012 af, Depth&gt; 1.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
3,138	39	>75% Grass cover, Good, HSG A
589	98	Paved parking, HSG A
3,727	48	Weighted Average
3,138		84.20% Pervious Area
589		15.80% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-2: Front-west**

Runoff = 0.02 cfs @ 12.00 hrs, Volume= 0.001 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
752	39	>75% Grass cover, Good, HSG A
752		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

**Summary for Subcatchment E-3: Rear**

Runoff = 1.99 cfs @ 11.98 hrs, Volume= 0.087 af, Depth&gt; 2.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
371	98	Paved parking, HSG A
1,712	98	Roofs, HSG A
9,022	39	>75% Grass cover, Good, HSG A
8,603	61	>75% Grass cover, Good, HSG B
19,708	55	Weighted Average
17,625		89.43% Pervious Area
2,083		10.57% Impervious Area

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Permeability of 15.0 in/hr  
Type II 24-hr 100-yr Rainfall=7.65"

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Page 26

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1: Front to street**

Runoff = 0.06 cfs @ 12.00 hrs, Volume= 0.003 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,828	39	>75% Grass cover, Good, HSG A
1,828		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-1A: Front to CB-1**

Runoff = 0.35 cfs @ 11.96 hrs, Volume= 0.018 af, Depth&gt; 6.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,342	98	Paved parking, HSG A
158	39	>75% Grass cover, Good, HSG A
1,500	92	Weighted Average
158		10.53% Pervious Area
1,342		89.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0	Direct Entry,				

**Summary for Subcatchment P-2: Front-west**

Runoff = 0.01 cfs @ 12.00 hrs, Volume= 0.001 af, Depth&gt; 0.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
382	39	>75% Grass cover, Good, HSG A
382		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

### Summary for Subcatchment P-3: Rear yard

Runoff = 1.66 cfs @ 11.98 hrs, Volume= 0.072 af, Depth> 2.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
7,495	61	>75% Grass cover, Good, HSG B
2,001	39	>75% Grass cover, Good, HSG A
3,921	39	>75% Grass cover, Good, HSG A
1,712	98	Roofs, HSG A
15,129	57	Weighted Average
13,417		88.68% Pervious Area
1,712		11.32% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

### Summary for Subcatchment P-4: Bldg/pavement

Runoff = 2.04 cfs @ 11.89 hrs, Volume= 0.089 af, Depth> 6.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
Type II 24-hr 100-yr Rainfall=7.65"

Area (sf)	CN	Description
1,588	98	Roofs, HSG A
200	98	Paved parking, HSG A
225	61	>75% Grass cover, Good, HSG B
1,068	98	Paved parking, HSG B
443	39	>75% Grass cover, Good, HSG A
288	39	>75% Grass cover, Good, HSG A
3,716	98	Paved parking, HSG A
7,528	91	Weighted Average
956		12.70% Pervious Area
6,572		87.30% Impervious Area

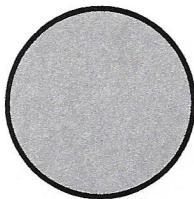
**Summary for Reach CB-3: HS-2**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 6.16" for 100-yr event  
 Inflow = 2.04 cfs @ 11.89 hrs, Volume= 0.089 af  
 Outflow = 1.37 cfs @ 12.00 hrs, Volume= 0.089 af, Atten= 33%, Lag= 6.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Max. Velocity= 7.73 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 3.01 fps, Avg. Travel Time= 0.0 min

Peak Storage= 2 cf @ 11.85 hrs  
 Average Depth at Peak Storage= 0.50'  
 Bank-Full Depth= 0.50' Flow Area= 0.2 sf, Capacity= 1.33 cfs

6.0" Round Pipe  
 n= 0.010 PVC, smooth interior  
 Length= 9.0' Slope= 0.0333 '/  
 Inlet Invert= 76.30', Outlet Invert= 76.00'

**Summary for Pond 1P: Rear Infiltration**

Inflow Area = 0.173 ac, 87.30% Impervious, Inflow Depth > 6.16" for 100-yr event  
 Inflow = 1.37 cfs @ 12.00 hrs, Volume= 0.089 af  
 Outflow = 0.46 cfs @ 12.06 hrs, Volume= 0.089 af, Atten= 66%, Lag= 3.4 min  
 Discarded = 0.46 cfs @ 12.06 hrs, Volume= 0.089 af  
 Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 75.82' @ 12.06 hrs Surf.Area= 945 sf Storage= 1,055 cf

Plug-Flow detention time= 12.9 min calculated for 0.089 af (100% of inflow)  
 Center-of-Mass det. time= 12.7 min ( 750.9 - 738.2 )

Volume	Invert	Avail.Storage	Storage Description
#1	74.00'	681 cf	10.00'W x 94.50'L x 2.50'H Prismatoid 2,363 cf Overall - 661 cf Embedded = 1,702 cf x 40.0% Voids
#2	74.50'	661 cf	18.0" Round CMP_Round 18" x 4 Inside #1 L= 93.5'
1,342 cf			Total Available Storage

Device	Routing	Invert	Outlet Devices
#1	Discarded	74.00'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.80'	18.0" Round Culvert L= 3.8' Ke= 0.900

Inlet / Outlet Invert= 76.00' / 79.80' S= -1.0000 '/' Cc= 0.900  
 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

**Discarded OutFlow** Max=0.46 cfs @ 12.06 hrs HW=75.81' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.46 cfs)

**Primary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=74.00' (Free Discharge)  
 ↗2=Culvert (Controls 0.00 cfs)

### Summary for Pond 2P: Front infiltration

Inflow Area = 0.043 ac, 71.31% Impervious, Inflow Depth > 5.16" for 100-yr event  
 Inflow = 0.36 cfs @ 11.96 hrs, Volume= 0.019 af  
 Outflow = 0.41 cfs @ 12.00 hrs, Volume= 0.019 af, Atten= 0%, Lag= 2.1 min  
 Discarded = 0.11 cfs @ 12.00 hrs, Volume= 0.016 af  
 Primary = 0.30 cfs @ 12.00 hrs, Volume= 0.002 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 79.79' @ 12.00 hrs Surf.Area= 318 sf Storage= 144 cf

Plug-Flow detention time= 11.3 min calculated for 0.019 af (100% of inflow)  
 Center-of-Mass det. time= 11.1 min ( 755.0 - 743.9 )

Volume	Invert	Avail.Storage	Storage Description
#1	78.50'	222 cf	Custom Stage Data (Conic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
78.50	10	0	0	10
79.00	51	14	14	52
80.00	427	209	222	431

Device	Routing	Invert	Outlet Devices
#1	Discarded	78.50'	15.000 in/hr Exfiltration over Wetted area
#2	Primary	79.75'	25.0' long Broad-Crested Rectangular Weir Head (feet) 1.50 Coef. (English) 1.50

**Discarded OutFlow** Max=0.11 cfs @ 12.00 hrs HW=79.79' (Free Discharge)  
 ↗1=Exfiltration (Exfiltration Controls 0.11 cfs)

**Primary OutFlow** Max=0.29 cfs @ 12.00 hrs HW=79.79' (Free Discharge)  
 ↗2=Broad-Crested Rectangular Weir (Weir Controls 0.29 cfs @ 0.30 fps)

**Summary for Link 1L: Cum.Discharge**

Inflow Area = 0.391 ac, 17.95% Impervious, Inflow Depth > 2.29" for 100-yr event

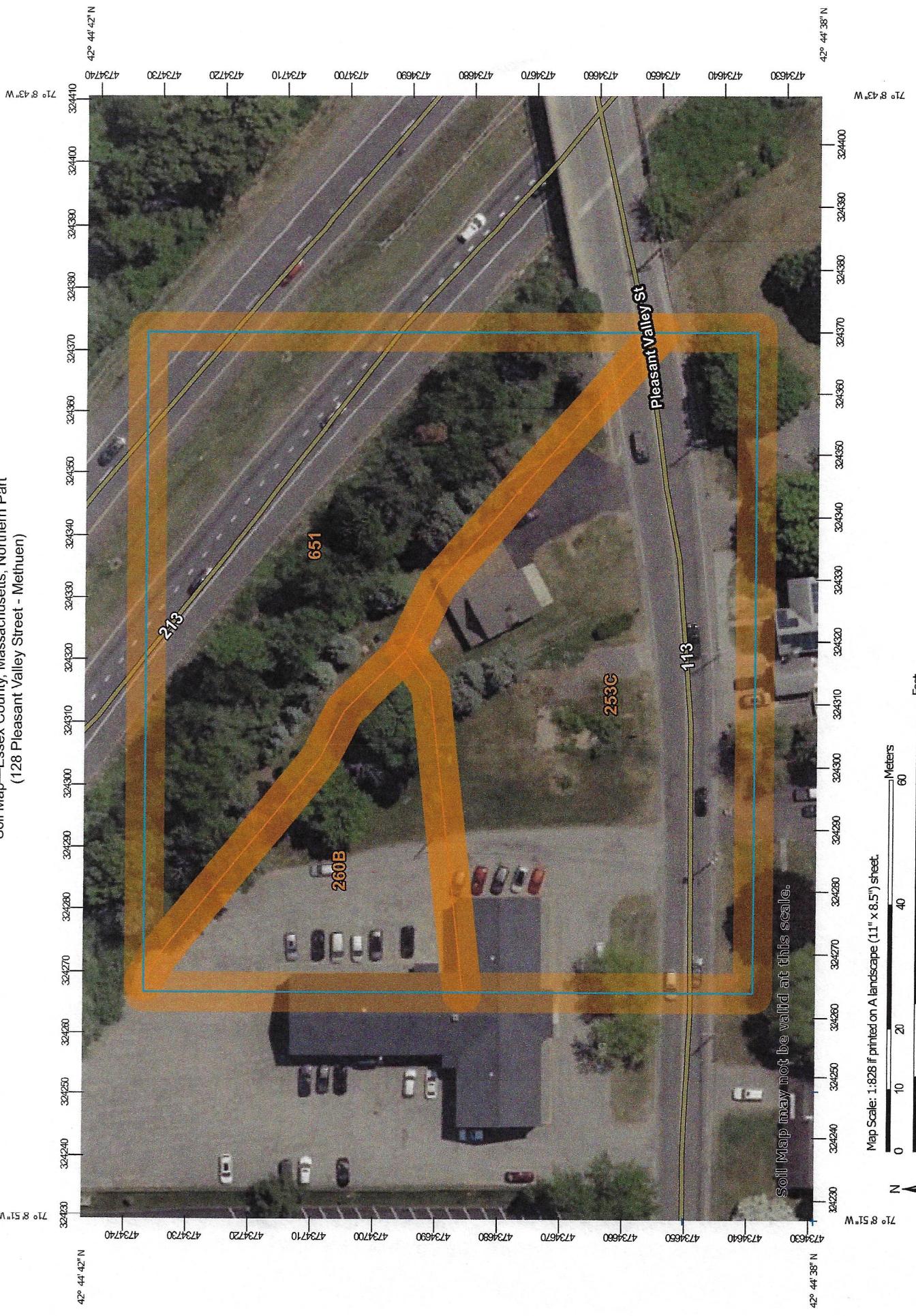
Inflow = 1.94 cfs @ 11.99 hrs, Volume= 0.075 af

Primary = 1.94 cfs @ 11.99 hrs, Volume= 0.075 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

**USDA SOILS INFORMATION**

Soil Map—Essex County, Massachusetts, Northern Part  
(128 Pleasant Valley Street - Methuen)



## MAP LEGEND

## MAP INFORMATION

Area of Interest (AOI)	
	Area of Interest (AOI)
	Soils
	Soil Map Unit Polygons
	Soil Map Unit Lines
	Soil Map Unit Points
Special Point Features	
	Blowout
	Borrow Pit
	Clay Spot
	Closed Depression
	Gravel Pit
	Gravelly Spot
	Landfill
	Lava Flow
	Marsh or swamp
	Mine or Quarry
	Miscellaneous Water
	Perennial Water
	Rock Outcrop
	Saline Spot
	Sandy Spot
	Severely Eroded Spot
	Sinkhole
	Slide or Slip
	Sodic Spot
Spoil Area	
	Stony Spot
	Very Stony Spot
	Wet Spot
	Other
Special Line Features	
	Streams and Canals
Water Features	
Transportation	
	Rails
	Interstate Highways
	US Routes
	Major Roads
	Local Roads
Background	
	Aerial Photography

The soil surveys that comprise your AOI were mapped at 1:15,800

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL: <http://websoilsurvey.gov>  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Essex County, Massachusetts, Northern Part  
Survey Area Data: Version 18, Sep 9, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 22, 2022—Jun 5, 2022

The orthophoto or outer base map on which the son lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
253C	Hinckley loamy sand, 8 to 15 percent slopes	1.2	44.9%
260B	Sudbury fine sandy loam, 3 to 8 percent slopes	0.4	14.9%
651	Udorthents, smoothed	1.0	40.2%
<b>Totals for Area of Interest</b>		<b>2.6</b>	<b>100.0%</b>

## Essex County, Massachusetts, Northern Part

### 253C—Hinckley loamy sand, 8 to 15 percent slopes

#### Map Unit Setting

*National map unit symbol:* 2svm9

*Elevation:* 0 to 1,480 feet

*Mean annual precipitation:* 36 to 71 inches

*Mean annual air temperature:* 39 to 55 degrees F

*Frost-free period:* 140 to 240 days

*Farmland classification:* Farmland of statewide importance

#### Map Unit Composition

*Hinckley and similar soils:* 85 percent

*Minor components:* 15 percent

*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### Description of Hinckley

##### Setting

*Landform:* Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

*Landform position (two-dimensional):* Shoulder, backslope, footslope, toeslope

*Landform position (three-dimensional):* Head slope, nose slope, side slope, crest, riser

*Down-slope shape:* Concave, convex, linear

*Across-slope shape:* Convex, linear, concave

*Parent material:* Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

##### Typical profile

*Oe - 0 to 1 inches:* moderately decomposed plant material

*A - 1 to 8 inches:* loamy sand

*Bw1 - 8 to 11 inches:* gravelly loamy sand

*Bw2 - 11 to 16 inches:* gravelly loamy sand

*BC - 16 to 19 inches:* very gravelly loamy sand

*C - 19 to 65 inches:* very gravelly sand

##### Properties and qualities

*Slope:* 8 to 15 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Excessively drained

*Runoff class:* Very low

*Capacity of the most limiting layer to transmit water*

*(Ksat):* Moderately high to very high (1.42 to 99.90 in/hr)

*Depth to water table:* More than 80 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)

*Available water supply, 0 to 60 inches:* Low (about 3.1 inches)



### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 4e

*Hydrologic Soil Group:* A

*Ecological site:* F144AY022MA - Dry Outwash

*Hydric soil rating:* No

### Minor Components

#### Merrimac

*Percent of map unit:* 5 percent

*Landform:* Kames, outwash plains, outwash terraces, moraines, eskers

*Landform position (two-dimensional):* Shoulder, backslope, footslope, toeslope

*Landform position (three-dimensional):* Head slope, nose slope, side slope, crest, riser

*Down-slope shape:* Convex

*Across-slope shape:* Convex

*Hydric soil rating:* No

#### Sudbury

*Percent of map unit:* 5 percent

*Landform:* Outwash deltas, moraines, outwash plains, kame terraces, outwash terraces

*Landform position (two-dimensional):* Backslope, footslope

*Landform position (three-dimensional):* Base slope, tread

*Down-slope shape:* Concave, linear

*Across-slope shape:* Concave, linear

*Hydric soil rating:* No

#### Windsor

*Percent of map unit:* 5 percent

*Landform:* Moraines, eskers, kames, outwash deltas, outwash terraces, outwash plains, kame terraces

*Landform position (two-dimensional):* Shoulder, backslope, footslope, toeslope

*Landform position (three-dimensional):* Head slope, nose slope, side slope, crest, riser

*Down-slope shape:* Concave, convex, linear

*Across-slope shape:* Convex, linear, concave

*Hydric soil rating:* No

## Data Source Information

Soil Survey Area: Essex County, Massachusetts, Northern Part

Survey Area Data: Version 19, Sep 10, 2023



Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

11/5/2023  
Page 2 of 2

## Essex County, Massachusetts, Northern Part

### 260B—Sudbury fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

*National map unit symbol:* vjsn

*Elevation:* 0 to 2,100 feet

*Mean annual precipitation:* 45 to 54 inches

*Mean annual air temperature:* 43 to 54 degrees F

*Frost-free period:* 145 to 240 days

*Farmland classification:* All areas are prime farmland

#### Map Unit Composition

*Sudbury and similar soils:* 80 percent

*Minor components:* 20 percent

*Estimates are based on observations, descriptions, and transects of  
the mapunit.*

#### Description of Sudbury

##### Setting

*Landform:* Terraces

*Landform position (two-dimensional):* Footslope

*Landform position (three-dimensional):* Tread

*Down-slope shape:* Linear

*Across-slope shape:* Concave

*Parent material:* Friable loamy eolian deposits over loose sandy  
glaciofluvial deposits derived from granite and gneiss

##### Typical profile

*O - 0 to 1 inches:* muck

*H2 - 1 to 5 inches:* fine sandy loam

*H3 - 5 to 21 inches:* sandy loam

*H4 - 21 to 27 inches:* loamy sand

*H5 - 27 to 60 inches:* Error

##### Properties and qualities

*Slope:* 3 to 8 percent

*Depth to restrictive feature:* More than 80 inches

*Drainage class:* Moderately well drained

*Capacity of the most limiting layer to transmit water (Ksat):* High  
(2.00 to 6.00 in/hr)

*Depth to water table:* About 18 to 36 inches

*Frequency of flooding:* None

*Frequency of ponding:* None

*Available water supply, 0 to 60 inches:* Low (about 4.7 inches)

##### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 2e

*Hydrologic Soil Group:* B

*Ecological site:* F144AY027MA - Moist Sandy Outwash



*Hydric soil rating:* No

#### **Minor Components**

##### **Merrimac**

*Percent of map unit:* 15 percent

*Hydric soil rating:* No

##### **Walpole**

*Percent of map unit:* 5 percent

*Landform:* Terraces

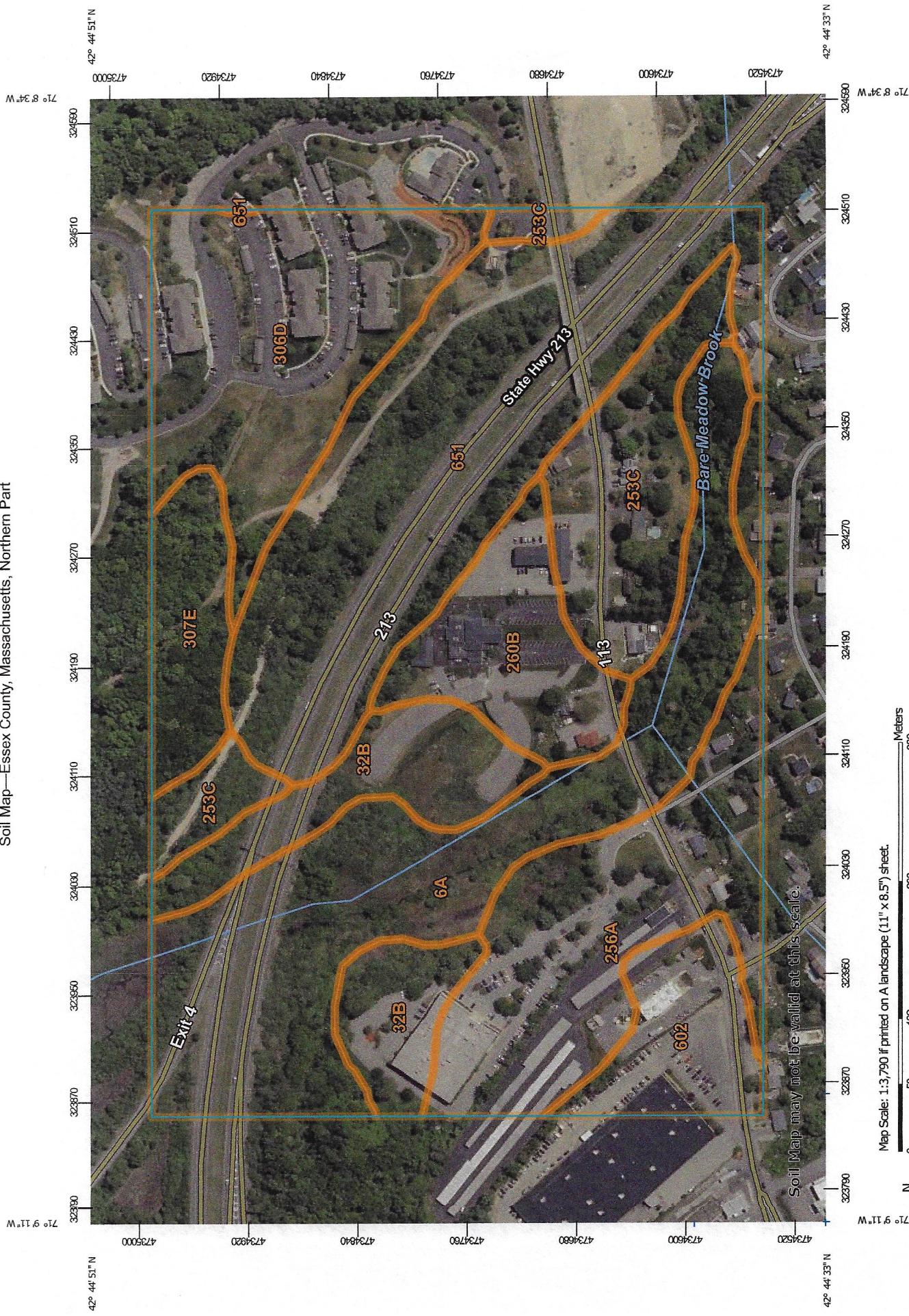
*Hydric soil rating:* Yes

### **Data Source Information**

Soil Survey Area: Essex County, Massachusetts, Northern Part

Survey Area Data: Version 19, Sep 10, 2023

Soil Map—Essex County, Massachusetts, Northern Part



Map Scale: 1:3 780 if printed on A4 landscape (11" x 8 5") sheet

—Meters  
300  
200  
100

670

N

USDA Natural Resources Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

## MAP LEGEND

<b>Area of Interest (AOI)</b>		Area of Interest (AOI)
<b>Soils</b>		Soil Map Unit Polygons
		Soil Map Unit Lines
		Soil Map Unit Points
<b>Special Point Features</b>		
Blowout		
Borrow Pit		
Clay Spot		
Closed Depression		
Gravel Pit		
Gravelly Spot		
Landfill		
Lava Flow		
Marsh or swamp		
Mine or Quarry		
Miscellaneous Water		
Perennial Water		
Rock Outcrop		
Saline Spot		
Sandy Spot		
Severely Eroded Spot		
Sinkhole		
Slide or Slip		
Sodic Spot		

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

**Warning: Soil Map may not be valid at this scale.**  
 Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

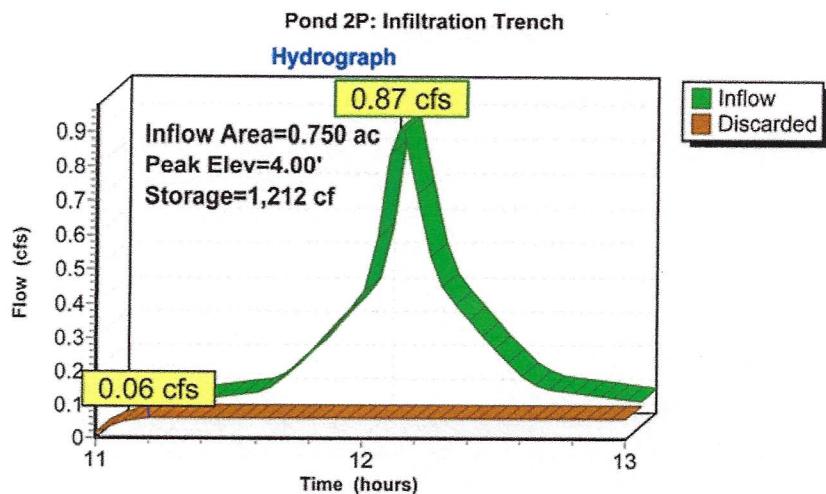
**Source of Map:** Natural Resources Conservation Service  
 Web Soil Survey URL:  
 Coordinate System: Web Mercator (EPSG:3857)  
 Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.  
 This product is generated from the USDA NRCS certified data as of the version date(s) listed below.  
**Soil Survey Area:** Essex County, Massachusetts, Northern Part  
**Survey Area Data:** Version 18, Sep 9, 2022  
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**Date(s) aerial images were photographed:** May 22, 2022—Jun 5, 2022  
 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
6A	Scarboro mucky fine sandy loam, 0 to 3 percent slopes	14.5	19.5%
32B	Wareham loamy sand, 3 to 8 percent slopes	6.0	8.2%
253C	Hinckley loamy sand, 8 to 15 percent slopes	7.0	9.4%
256A	Deerfield loamy fine sand, 0 to 3 percent slopes	9.8	13.3%
260B	Sudbury fine sandy loam, 3 to 8 percent slopes	4.5	6.1%
306D	Paxton fine sandy loam, 15 to 25 percent slopes, very stony	9.8	13.2%
307E	Paxton fine sandy loam, 25 to 35 percent slopes, extremely stony	2.9	3.9%
602	Urban land	3.4	4.6%
651	Udorthents, smoothed	16.1	21.7%
<b>Totals for Area of Interest</b>		<b>74.1</b>	<b>100.0%</b>

**PERMEABILITY TESTS**

Type III 24-hr Rainfall=1.29"



**Table 2.3.3. 1982 Rawls Rates<sup>18</sup>**

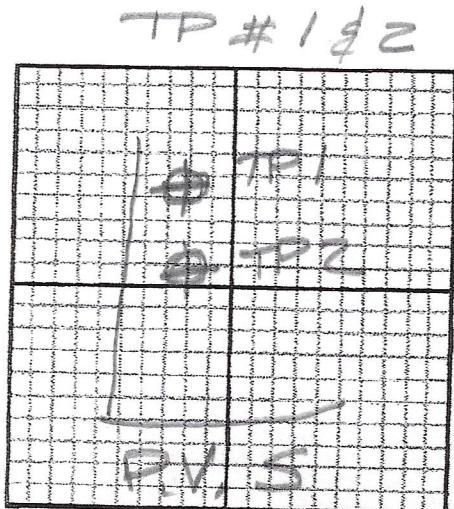
Texture Class	NRCS Hydrologic Soil Group (HSG)	Infiltration Rate Inches/Hour
Sand	A	8.27
Loamy Sand	A	2.41
Sandy Loam	B	1.02
Loam	B	0.52
Silt Loam	C	0.27
Sandy Clay Loam	C	0.17
Clay Loam	D	0.09
Silty Clay Loam	D	0.06
Sandy Clay	D	0.05
Silty Clay	D	0.04
Clay	D	0.02

<sup>18</sup> Rawls, Brakensiek and Saxton, 1982

## GP FIELD DATA SHEET

Date 8/7/23 Investigator CAELLOS QUINTAL  
 Site Location 128 PLEASANT VALLEY ST METHUEN  
 Dominant Soil Type(s) SUDBURY FINE SANDY LOAM

Site Map:



Soil Profile Description (horizon depth, texture, structure, color, etc.):

Depth

Description

6"	A	TOP SOIL-3L-10YR4/3
12"	B	SUB SOIL-SL-10YR5/4
7"	C1	COARSE LS 2.5Y5/4
18"	C2	GRAVELLY LS

Presence of special soil conditions (mottling, water table depth, hardpan, induration, compacted layers, etc.):

NO WATER  
NO MOTTLES

Comments and Notes (topography, slope, vegetation, etc.):

## Guelph Permeameter Data Sheet

Investigator: CARLOS QUINTAL

Date: 8/7/23

Location: 128 P. V. ST

Test Id: PT-2

Depth of hole: 40" Radius: 3 cm (standard calcs assume 3 cm radius)

Reservoirs used during test (check one): Combined:  Inner only: \_\_\_\_\_

Reservoir constant used: 35.22

Steady rate for 3 consecutive readings ( $R_1$ ):

16.6

Water level in well = 10 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoi r <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh</i> / <i>Dt</i>
0		25		
:14	0,23	30	5	21,42
:27	0,22	35	5	23,08
:42	0,25	40	5	20,00
:53	0,18	45	5	27,27
1:10	0,28	50	5	17,65
1:23	0,22	55	5	23,08
1:38	0,25	60	5	20,00
1:52	0,23	65	5	21,43
2:06	0,23	70	5	21,43
2:20	0,23	75	5	21,43

Steady rate for 3 consecutive readings ( $R_2$ ):

217

**Comments:**

$$K_f = 0,577 \text{ in/mm} = 34,62 \text{ in/lb}$$

## Guelph Permeameter Data Sheet

Investigator: CARLOS QUINTAL Date: 8/7/23

Location: 128 PLEASANT VALLEY Test Id: PA1#1

Depth of hole: 36" Radius: 3 cm (standard calcs assume 3 cm radius)

Reservoirs used during test (check one): Combined:  Inner only:

Reservoir constant used: 35, 22

Steady rate for 3 consecutive readings ( $R_1$ ): 16.5

Steady rate for 3 consecutive readings ( $R_2$ ):

### Comments:

$$K_f = 0.572 \text{ in/min} = 34.32 \text{ in/hr}$$

# Soilmoisture Guelpth Permeameter Calculations

Input  
Result

Head #1	Head #2	Average															
<p>Reservoir Type(enter "1" for Combined and "2" for inner reservoir): <b>1</b></p> <p>Enter water Head height ("H" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>3</b></p> <p>Enter the soil texture-structure category (enter one of the below numbers): <b>4</b></p> <p>1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 21.4000</b></p> <p>Res Type: 35.2 H: 5 a: 3 H/a: 3.3333 a*: 0.38 C0.01: 1.2154 C0.02: 1.2502 C0.12: 1.2875 C0.36: 1.2975 C: 1.2875 R: 21.4000 Q: 12.592 p: 3.415 <math>\phi_m = 6.35E-02 \text{ (m}^2/\text{min)}</math></p> <p>Calculation formula related to one-head and two-head methods. Where <math>R</math> is steady-state rate of fall of water in reservoir (cm/s), <math>K_f</math> is soil saturated hydraulic conductivity (cm/s), <math>\phi_m</math> is soil matrix flux potential (cm/s), <math>a^*</math> is Macroscopic capillary length parameter (from Table 2), <math>a</math> is Borehole radius (cm), <math>H_1</math> is the first head of water established in borehole (cm), <math>H_2</math> is the second head of water established in borehole (cm) and C is S-shape factor (from Table 2).</p> <p><b>Soil Texture-Structure Category</b></p> <table border="1"> <thead> <tr> <th>alpha (cm)</th> <th>alpha (cm)</th> <th>Shape Factor</th> </tr> </thead> <tbody> <tr> <td>0.01</td> <td><math>\frac{H_1/a}{H_2/a}</math></td> <td><math>C_1 = \frac{(1.02 + 0.118(H_1/a))}{(2.02 + 0.118(H_2/a))}</math> <math>C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}</math></td> </tr> <tr> <td>0.04</td> <td><math>\frac{H_1/a}{H_2/a}</math></td> <td><math>C_1 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}</math> <math>C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}</math></td> </tr> <tr> <td>0.12</td> <td><math>\frac{H_1/a}{H_2/a}</math></td> <td><math>C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}</math> <math>C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}</math></td> </tr> <tr> <td>0.36</td> <td><math>\frac{H_1/a}{H_2/a}</math></td> <td><math>C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}</math> <math>C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}</math></td> </tr> </tbody> </table> <p>Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils.</p> <p>Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p>	alpha (cm)	alpha (cm)	Shape Factor	0.01	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(1.02 + 0.118(H_1/a))}{(2.02 + 0.118(H_2/a))}$ $C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$	0.04	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$ $C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$	0.12	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$ $C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$	0.36	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$ $C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$	<p>Reservoir Type (enter "1" for Combined and "2" for inner reservoir): <b>1</b></p> <p>Enter water Head height ("H" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>3</b></p> <p>Enter the soil texture-structure category (enter one of the below numbers): <b>3</b></p> <p>1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 16.0000</b></p> <p>Res Type: 35.2 H: 10 a: 3 H/a: 3.3333 a*: 0.38 C: 1.28754 Q: 12.5818 <math>K_f = 1.33E-02 \text{ cm/sec}</math> <math>\phi_m = 6.35E-02 \text{ (m}^2/\text{min)}</math></p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 24.4000</b></p> <p>Res Type: 35.2 H: 10 a: 3 H/a: 3.3333 a*: 0.38 C: 1.28754 Q: 12.5818 <math>K_f = 1.33E-02 \text{ cm/sec}</math> <math>\phi_m = 6.35E-02 \text{ (m}^2/\text{min)}</math></p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 24.4000</b></p> <p>Res Type: 2.18 H1/a: 1.66667 H2/a: 3.33333 C1&lt;0.01: 0.05949 C2&lt;0.01: 0.05949 C3&lt;0.04: 0.04096 C4&lt;0.04: 0.04096 C1&lt;0.12: 0.0515 C2&lt;0.12: 0.0515 C3&lt;0.36: 0.03035 C4&lt;0.36: 0.03035 <math>K_f = 1.17E-04 \text{ cm/sec}</math> <math>\phi_m = 6.39E-03 \text{ cm/min}</math> <math>2.75E-03 \text{ inch/min}</math> <math>4.59E-05 \text{ inch/sec}</math> <math>\phi_m = 1.445E-02 \text{ (m}^2/\text{min)}</math></p>	<p>Reservoir Type (enter "1" for Combined and "2" for inner reservoir): <b>1</b></p> <p>Enter water Head height ("H" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>5</b></p> <p>Enter the first water Head Height ("H1" in cm): <b>5</b></p> <p>Enter the second water Head Height ("H2" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>3</b></p> <p>Enter the soil texture-structure category (enter one of the below numbers): <b>3</b></p> <p>1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 16.0000</b></p> <p>Res Type: 2.18 H1/a: 1.66667 H2/a: 3.33333 C1&lt;0.01: 0.05949 C2&lt;0.01: 0.05949 C3&lt;0.04: 0.04096 C4&lt;0.04: 0.04096 C1&lt;0.12: 0.0515 C2&lt;0.12: 0.0515 C3&lt;0.36: 0.03035 C4&lt;0.36: 0.03035 <math>K_f = 1.17E-04 \text{ cm/sec}</math> <math>\phi_m = 6.39E-03 \text{ cm/min}</math> <math>2.75E-03 \text{ inch/min}</math> <math>4.59E-05 \text{ inch/sec}</math> <math>\phi_m = 1.445E-02 \text{ (m}^2/\text{min)}</math></p>
alpha (cm)	alpha (cm)	Shape Factor															
0.01	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(1.02 + 0.118(H_1/a))}{(2.02 + 0.118(H_2/a))}$ $C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$															
0.04	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$ $C_2 = \frac{(1.992 + 0.091(H_1/a))}{(1.992 + 0.091(H_2/a))}$															
0.12	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$ $C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$															
0.36	$\frac{H_1/a}{H_2/a}$	$C_1 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$ $C_2 = \frac{(2.074 + 0.093(H_1/a))}{(2.074 + 0.093(H_2/a))}$															

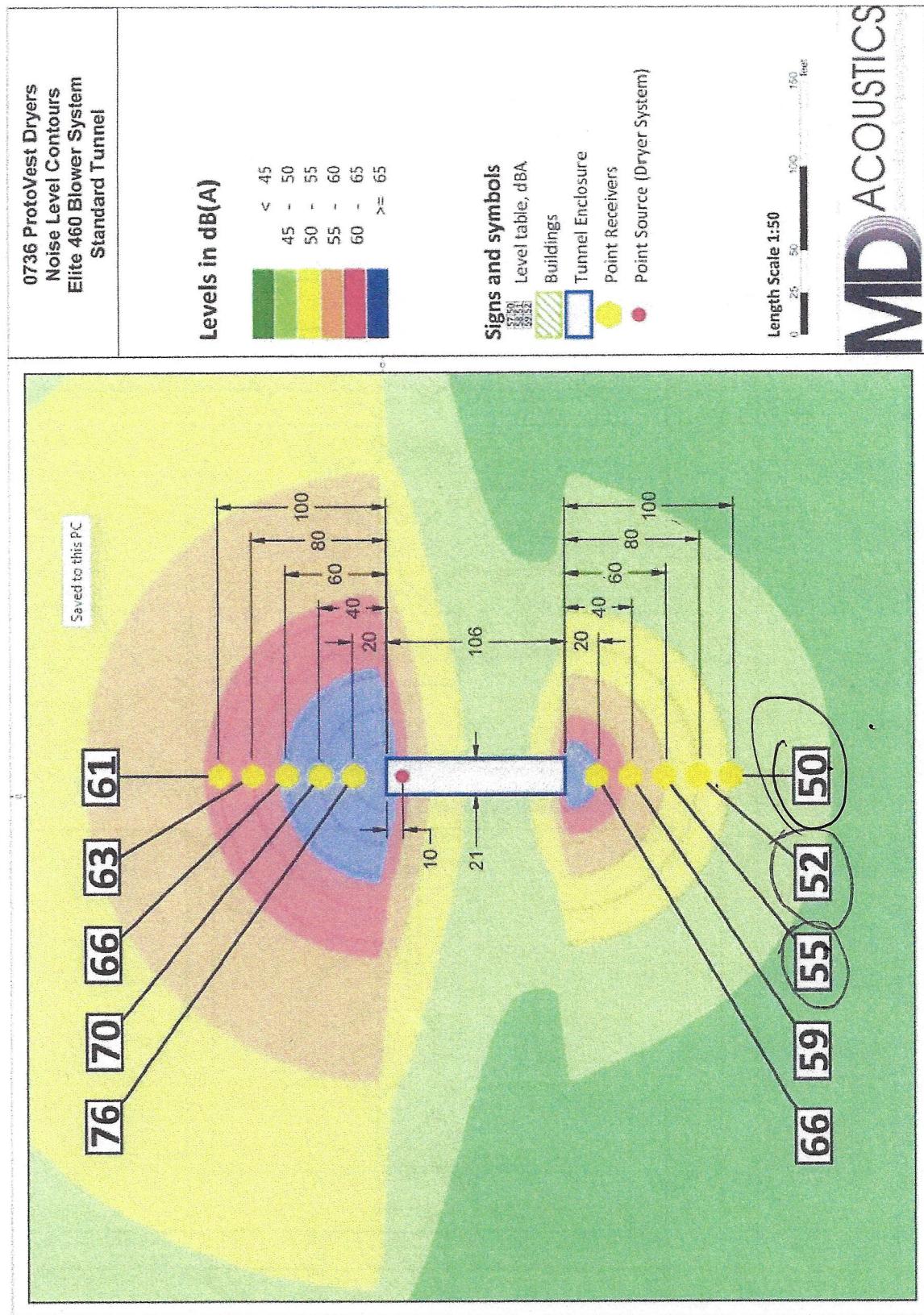
Two Head Method	
<p>Reservoir Type (enter "1" for Combined and "2" for inner reservoir): <b>1</b></p> <p>Enter water Head height ("H" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>3</b></p> <p>Enter the soil texture-structure category (enter one of the below numbers): <b>3</b></p> <p>1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 16.0000</b></p> <p>Res Type: 2.18 H1/a: 1.66667 H2/a: 3.33333 C1&lt;0.01: 0.05949 C2&lt;0.01: 0.05949 C3&lt;0.04: 0.04096 C4&lt;0.04: 0.04096 C1&lt;0.12: 0.0515 C2&lt;0.12: 0.0515 C3&lt;0.36: 0.03035 C4&lt;0.36: 0.03035 <math>K_f = 1.17E-04 \text{ cm/sec}</math> <math>\phi_m = 6.39E-03 \text{ cm/min}</math> <math>2.75E-03 \text{ inch/min}</math> <math>4.59E-05 \text{ inch/sec}</math> <math>\phi_m = 1.445E-02 \text{ (m}^2/\text{min)}</math></p>	<p>Reservoir Type (enter "1" for Combined and "2" for inner reservoir): <b>1</b></p> <p>Enter water Head height ("H" in cm): <b>10</b></p> <p>Enter the Borehole Radius ("a" in cm): <b>5</b></p> <p>Enter the soil texture-structure category (enter one of the below numbers): <b>3</b></p> <p>1. Compacted, Structure-less, clayey or silty materials such as landfill caps and liners, lacustrine or marine sediments, etc. 2. Soils which are both fine textured (clayey or silty) and unstructured; may also include some fine sands. 3. Most structured soils from clays through loams; also includes unstructured medium and fine sands. The category most frequently applicable for agricultural soils. 4. Coarse and gravelly sands; may also include some highly structured soils with large and/or numerous cracks, macropores, etc.</p> <p><b>Steady State Rate of Water Level Change ("R" in cm/min): 16.0000</b></p> <p>Res Type: 2.18 H1/a: 1.66667 H2/a: 3.33333 C1&lt;0.01: 0.05949 C2&lt;0.01: 0.05949 C3&lt;0.04: 0.04096 C4&lt;0.04: 0.04096 C1&lt;0.12: 0.0515 C2&lt;0.12: 0.0515 C3&lt;0.36: 0.03035 C4&lt;0.36: 0.03035 <math>K_f = 1.17E-04 \text{ cm/sec}</math> <math>\phi_m = 6.39E-03 \text{ cm/min}</math> <math>2.75E-03 \text{ inch/min}</math> <math>4.59E-05 \text{ inch/sec}</math> <math>\phi_m = 1.445E-02 \text{ (m}^2/\text{min)}</math></p>

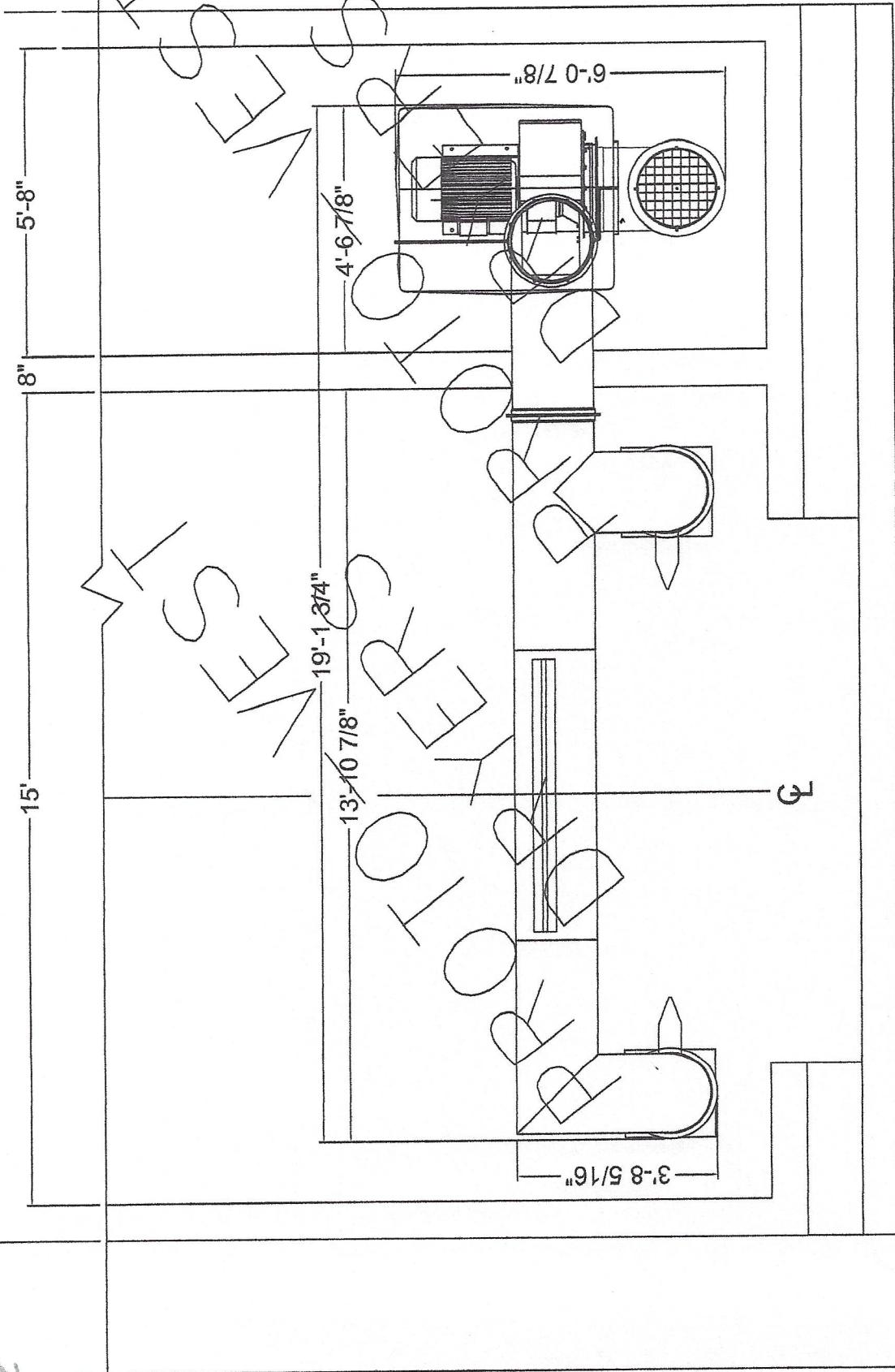


**EQUIPMENT NOISE**

# Exhibit A

## Elite 460 Noise Levels





SIGN TO CONFIRM MEASUREMENTS OF YOUR REQUIREMENTS:  X  
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TITLE: CUSTOM MAG WINDSHEAR A.T. W/ SIL. PKG PLAN VIEW BLOWER ON DRIVER SIDE		Proto-Vest Dryers
CAD DRAWING NAME: WINDSHEAR DRIVER SIDE BLOWER ROOM		
LAST DATE EDITED: 10/16/23	BY: RI	
DRAWN BY: A. AVTIA	SCALE: NONE	
DATE CREATED: 2/11/19	SHEET: 1 OF 2	



INTERNATIONAL DRYING  
CORPORATION

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### THE FIRST "ULTRA QUIET" DRYING SYSTEM

- ✓ Patent pending Reverse flow technology
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# Stealth Predator Ultra-Quiet Drying System Specifications

## 30HP System - Total Sound 60Hz

## 80HP System - Total Sound 60Hz

Q = sound source

65 dBA at Q=1, 30 feet

69.4 dBA at Q=1, 30 feet

61.8 dBA at Q=1, 45 feet

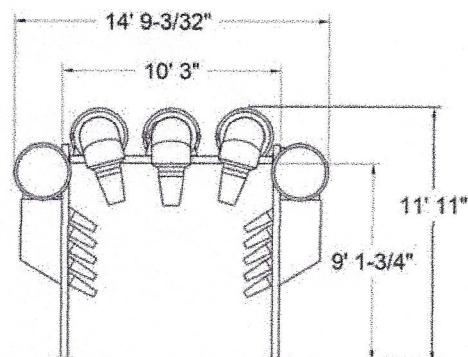
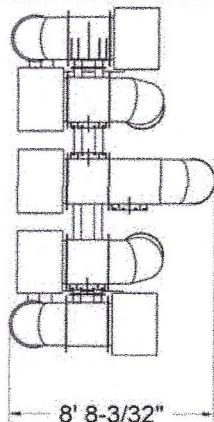
66.5 dBA at Q=1, 45 feet

60.2 dBA at Q=1, 55 feet

64.9 dBA at Q=1, 55 feet

Meets OSHA Sound Exposure Requirements

✓ The Stealth Predator features patent pending "Reverse flow air technology" which creates the first "Ultra-Quiet Dryer" and is the most powerful Ultra Quiet Dryer ever designed.



## SPECIFICATIONS

15' 2" Bay Width  
12' 0" Ceiling Height  
96" Standard Clearance

Ducts-Stainless Steel  
Molded Aluminum Impellers  
Stainless Steel Motor Housings

Closed cell foam nozzles available in red, blue, black

Slotted flanges for adjustability of air outlet and air intake direction

**TRAFFIC REPORT**

# MEMORANDUM

**TO:** Mr. Carlos Quintal  
CAQ Engineering Associates  
733 Turnpike Street, No. 261  
North Andover, MA 01845

**FROM:** Mr. Jeffrey S. Dirk, P.E.\*<sup>JSD</sup>, PTOE, FITE  
Managing Partner and  
Mr. Matthew P. Pelletier  
Transportation Engineer  
Vanasse & Associates, Inc.  
35 New England Business Center Drive  
Suite 140  
Andover, MA 01810-1066  
(978) 269-6830  
[jdirk@rdva.com](mailto:jdirk@rdva.com)

*\*Professional Engineer in CT, MA, ME, NH, RI, and VA*

**DATE:** October 31, 2023

**RE:** 9829

**SUBJECT:** Transportation Impact Assessment  
Proposed Car Wash – 128 Pleasant Valley Street (Route 113)  
Methuen, Massachusetts

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Vanasse & Associates, Inc. (VAI) has conducted a Transportation Impact Assessment (TIA) in order to determine the potential impacts on the transportation infrastructure associated with the proposed construction of an automated car wash to be located at 128 Pleasant Valley Street (Route 113) in Methuen, Massachusetts (hereafter referred to as the “Project”). This study evaluates the following specific areas as they relate to the Project: i) access requirements; ii) potential off-site improvements; and iii) safety considerations; and identifies and analyzes existing traffic conditions and future traffic conditions, both with and without the Project along Route 113. Based on this assessment, we have concluded the following with respect to the Project:

1. Using trip-generation statistics published by the Institute of Transportation Engineers (ITE),<sup>1</sup> the Project is expected to generate approximately 416 vehicle trips on an average weekday (two-way volume over the operational day of the Project), with 31 vehicle trips expected during the weekday morning peak hour, 21 vehicle trips expected during the weekday evening peak hour, and 46 vehicle trips expected during the Saturday midday peak hour;
2. The Project will not result in a significant impact (increase) on motorist delays or vehicle queuing over Existing or anticipated future conditions without the Project (No-Build conditions), with all movements along Route 113 approaching the Project site driveway shown to continue to operate at level-of-service (LOS) A with negligible vehicle queuing;
3. All movements exiting the Project site driveway to Route 113 are predicted to operate at LOS C during the peak hours with vehicle queues of up to one (1) vehicle predicted;

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<sup>1</sup>*Trip Generation*, 11<sup>th</sup> Edition; Institute of Transportation Engineers; Washington, DC; 2021.



4. No apparent safety deficiencies were noted with respect to the motor vehicle crash history in the vicinity of the Project site; and
5. Lines of sight at the intersections of the Project site driveways with Route 113 were found to exceed or can be made to exceed the recommended minimum distance for the intersections to operate in a safe and efficient manner based on the appropriate approach speed.

In consideration of the above, we have concluded that the Project can be accommodated within the confines of the existing transportation infrastructure in a safe and efficient manner with the implementation of the recommendations defined herein.

The following details our assessment of the Project.

### **PROJECT DESCRIPTION**

The Project will entail the construction of a 1,500 square foot (sf), single-tunnel, automated car wash to be located at 128 Pleasant Valley Street (Route 113) in Methuen, Massachusetts. The Project site encompasses approximately  $0.32\pm$  acres of previously disturbed land that is bound by Route 213 to the north; Route 113 to the south; a residential property to the east; and a commercial property to the west.



Source: Google Earth.

Access to the Project site will be provided by way of two driveways that will intersect the north side of Route 113 along the property frontage. The eastern driveway will serve as a one-way entrance drive, with the west driveway serving as the corresponding exit drive. Off-street parking will be provided for three (3) vehicles, which exceeds the parking requirements specified in Section VII603, *Parking and Loading Requirements*, of the City of Methuen Comprehensive Zoning Ordinance.<sup>2</sup>

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<sup>2</sup>One (1) parking space per 1,200 sf is required for a “Warehouse, Public Utility Station, in house Repair Garage, and Other Uses”.



## **STUDY METHODOLOGY**

This study was prepared in consultation with the Massachusetts Department of Transportation (MassDOT) and the City of Methuen; was performed in accordance with MassDOT's *Transportation Impact Assessment (TIA) Guidelines* and the standards of the Traffic Engineering and Transportation Planning professions for the preparation of such reports; and was conducted in three distinct stages.

The first stage involved an assessment of existing conditions in the study area and included an inventory of roadway geometrics; pedestrian and bicycle facilities; on-street parking; public transportation services; observations of traffic flow; and collection of pedestrian, bicycle, and vehicle counts.

In the second stage of the study, future traffic conditions were projected and analyzed. Specific travel demand forecasts for the Project were assessed along with future traffic demands due to expected traffic growth independent of the Project. A seven-year time horizon was selected for analyses consistent with MassDOT guidelines. The analysis conducted in stage two identifies existing or projected future capacity, safety, and access issues, as these areas relate to the transportation infrastructure.

The third stage of the study presents and evaluates measures to address deficiencies in the transportation infrastructure, if any, identified in stage two of the study.

## **EXISTING CONDITIONS**

A comprehensive field inventory of existing conditions within the study area was conducted in September 2023. This inventory included the collection of traffic-volume data and vehicle travel speed measurements, as well as a review of existing pedestrian and bicycle accommodations, public transportation services, and motor vehicle crash data. The following summarizes existing conditions within the study area.

### **Roadway**

#### **Pleasant Valley Street (Route 113)**

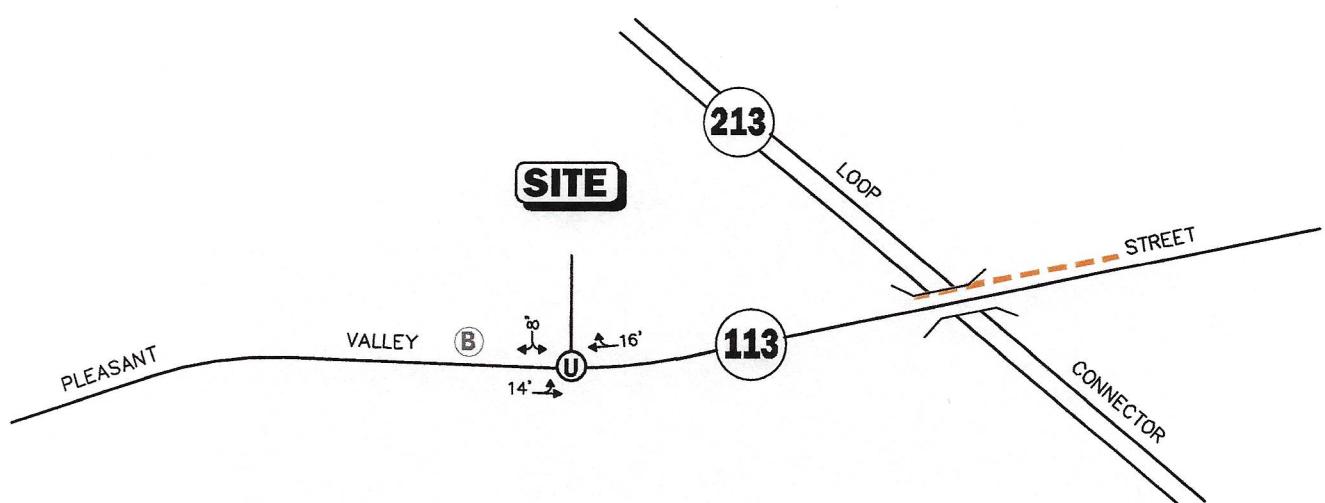
- Two-lane urban minor arterial roadway under City jurisdiction;
- Traverses the study area in a general east-west direction;
- Provides two 13- to 16-foot wide travel lanes that are separated by a double-yellow centerline with 1- to 5-foot wide marked shoulders in the vicinity of the Project site;
- The posted speed limit is 30 miles per hour (mph) in the vicinity of the Project site;
- Sidewalks are not provided along Route 113 within the study area;
- Illumination is provided by way of streetlights mounted on wood poles; and
- Land use within the study area consists of the Project site, residential and commercial properties, and areas of open and wooded space.

### **Intersection**

Table 1 and Figure 1 summarize existing lane use, traffic control, and pedestrian and bicycle accommodations at the study area intersection as observed in September 2023.

**Legend:**

- (U) Unsignalized Intersection
- (B) Bus Stop
- Sidewalk
- XX' → Lane Use and Travel Lane Width



Not To Scale



**Figure 1**

**Existing Intersection Lane Use, Travel Lane Width, and Pedestrian Facilities**

**Table 1**  
**STUDY AREA INTERSECTION DESCRIPTION**

Intersection	Traffic Control Type <sup>a</sup>	No. of Travel Lanes Provided	Shoulder Provided? (Yes/No/Width)	Pedestrian Accommodations? (Yes/No/Description)	Bicycle Accommodations? (Yes/No/Description)
Rte. 113/ Existing Site Driveway	S	1 general-purpose travel lane provided on all approaches	Yes; 1 to 5 feet on Rte. 113	No	Yes; shared traveled-way <sup>b</sup> on Rte. 113

<sup>a</sup>S = assumed stop control for driveway.

<sup>b</sup>Combined shoulder and travel lane width equal to or exceeding 14 feet.

### **Existing Traffic Volumes**

In order to determine existing traffic-volume demands and flow patterns within the study area, automatic traffic recorder (ATR) counts were completed in September 2023. The ATR counts were conducted on Route 113 at the Project site on September 21<sup>st</sup> and 22<sup>nd</sup>, 2023 (Thursday and Friday, inclusive), and on Saturday, September 30, 2023, in order to record weekday and Saturday traffic conditions over an extended period.

In order to evaluate the potential for seasonal fluctuation of traffic volumes within the study area, MassDOT weekday seasonal factors for Urban Groups 4-7 roadways (minor arterials, major and minor collectors, and local roads and streets, which includes the functional classification of Route 113) were reviewed.<sup>3</sup> Based on a review of this data, it was determined that traffic volumes for the month of September are approximately 8.7 percent above average-month conditions. As such, a seasonal adjustment was not required as the September traffic volumes are higher than those under average-month conditions.

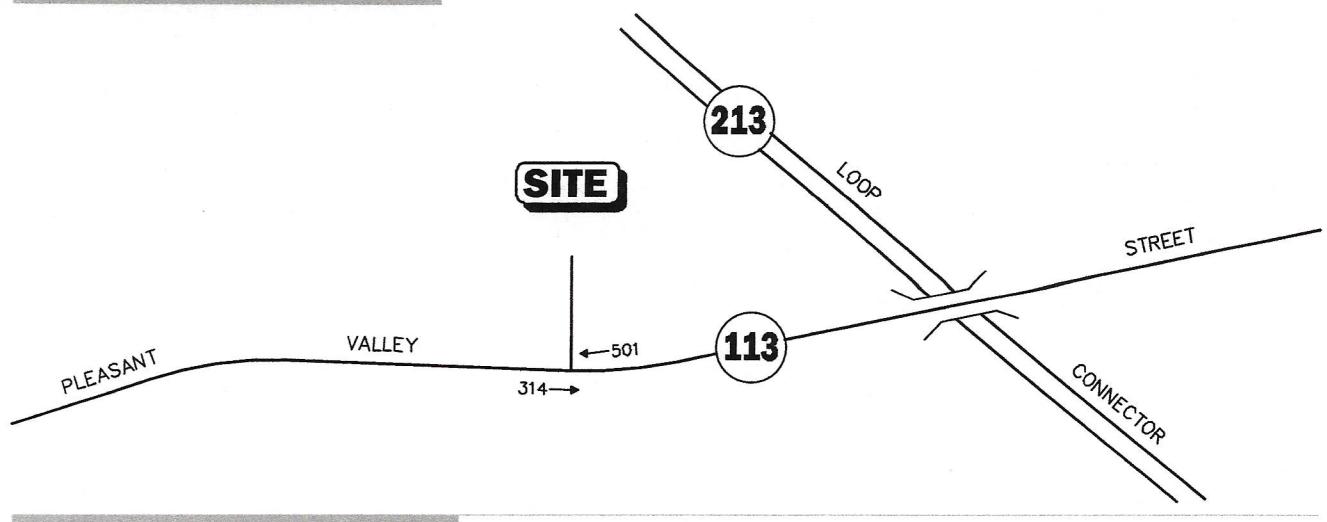
Based on current guidance from MassDOT,<sup>4</sup> pandemic-related adjustments to traffic counts performed after March 2022 are no longer required except in locations where the predominant land use consists of offices or similar uses. Given that the predominant land use within the study area is residential/commercial, a pandemic-related adjustment was not required.

The 2023 Existing traffic volumes are summarized in Table 2, with the weekday morning, weekday evening, and Saturday midday peak-hour traffic volumes graphically depicted on Figure 2. Note that the peak-hour traffic volumes presented in Table 2 were obtained from the aforementioned figure.

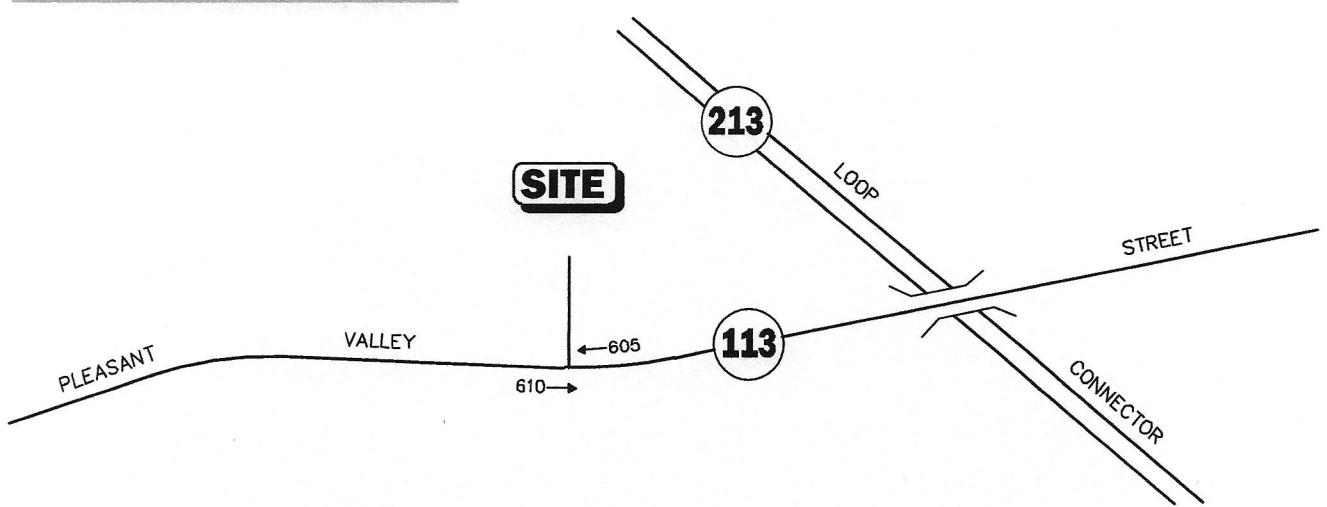
<sup>3</sup>MassDOT Statewide Traffic Data Collection; 2019 Weekday Seasonal Factors, Group U4-7.

<sup>4</sup>*Traffic and Safety Engineering 25% Design Submission Guidelines*; MassDOT; Revised March 31, 2022.

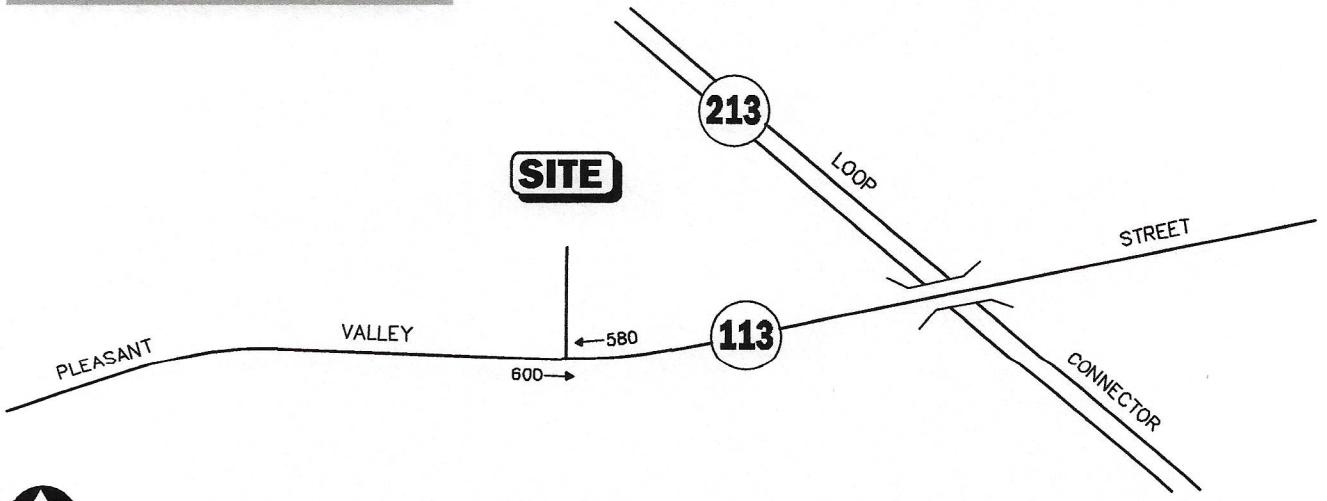
WEEKDAY MORNING PEAK HOUR



WEEKDAY EVENING PEAK HOUR



SATURDAY MIDDAY PEAK HOUR



Not To Scale



Figure 2

2023 Existing  
Peak-Hour Traffic Volumes

**Table 2**  
**2023 EXISTING TRAFFIC VOLUMES**

Location/Peak Hour	AWT <sup>a</sup>	Saturday <sup>b</sup>	VPH <sup>c</sup>	K Factor <sup>d</sup>	Directional Distribution <sup>e</sup>
<i>Route 113, west of Route 213:</i>					
Weekday Morning (7:30 – 8:30 AM)	13,660	12,605	--	--	--
Weekday Evening (4:30 – 5:30 PM)	--	--	815	6.0	61.5% WB
Saturday Midday (12:15 – 1:15 PM)	--	--	1,215	8.9	50.2% EB
	--	--	1,180	9.4	50.8% EB

<sup>a</sup>Average weekday traffic in vehicles per day.

<sup>b</sup>Average Saturday traffic in vehicles per day.

<sup>c</sup>Vehicles per hour.

<sup>d</sup>Percent of daily traffic occurring during the peak hour.

<sup>e</sup>Percent traveling in peak direction.

EB = eastbound, WB = westbound.

As can be seen in Table 2, Route 113 in the vicinity of the Project site was found to accommodate approximately 13,660 vehicles on an average weekday and approximately 12,605 vehicles on a Saturday (two-way, 24-hour volumes), with approximately 815 vehicles per hour (vph) during the weekday morning peak hour, 1,215 vph during the weekday evening peak hour and 1,180 vph during the Saturday midday peak hour.

### **Pedestrian and Bicycle Facilities**

A comprehensive field inventory of pedestrian and bicycle facilities within the study area was undertaken in September 2023. The field inventory consisted of a review of the location of sidewalks and pedestrian crossing locations along the study roadways and at the study intersections, as well as the location of existing and planned future bicycle facilities. Sidewalks are not provided along Route 113 in the vicinity to the Project site. To the east of the Project site, a sidewalk is provided along the north side of Route 113 across the bridge over Route 213 that extends to the driveway to the Summit Place apartments. Formal bicycle facilities are not provided within the study area; however, Route 113 provides sufficient width (combined travel lane and shoulder) to support bicycle travel in a shared traveled-way configuration (i.e., motor vehicles and bicyclists sharing the roadway).<sup>5</sup>

### **Public Transportation**

Public transportation services are provided within the study area by the Merrimack Valley Regional Transit Authority (MVRTA). The MVRTA provides fixed-route bus service along Route 113 adjacent to the Project site by way of bus Route 1, *Lawrence-Methuen-Haverhill*, which provides service within downtown Lawrence, downtown Haverhill, and Methuen. The Route 1 bus serves Haverhill Station on the Massachusetts Bay Transportation Authority (MBTA) Commuter Rail system (Haverhill Line) and also stops within 1 mile of the Lawrence Station (also on Haverhill Line), which provides service to North Station in Boston. The closest regular stop to the Project site for the Route 1 bus is located at 126 Pleasant Valley Street, which is approximately 150 feet to the west of the Project site (an approximate 1- to 2-minute walking distance). In addition to regular stops, MVRTA buses operate in a flag-stop mode,

<sup>5</sup>A minimum combined travel lane and paved shoulder width of 14 feet is required to support bicycle travel in a shared traveled-way condition.



where a passenger can request service (pick-up or drop-off) along the regular service route where it is safe to do so by signaling to the driver. The MVRTA also provides Dial-a-Ride paratransit services by way of the Ring & Ride program for eligible people who cannot use fixed-route transit all or some of the time due to a physical, cognitive, or mental disability in compliance with the Americans with Disabilities Act (ADA).

The public transportation schedules and fare information are attached.

### **Spot Speed Measurements**

Vehicle travel speed measurements were performed on Route 113 in the vicinity of the Project site in conjunction with the automatic traffic recorder (ATR) counts. Table 3 summarizes the vehicle travel speed measurements.

**Table 3**  
**VEHICLE TRAVEL SPEED MEASUREMENTS**

	Route 113	
	Eastbound	Westbound
Mean Travel Speed (mph)	32	36
85 <sup>th</sup> Percentile Speed (mph)	37	41
Posted Speed Limit (mph)	30	30

mph = miles per hour.

As can be seen in Table 3, the mean vehicle travel speed along Route 113 in the vicinity of the Project site was found to be 32 mph in the eastbound direction and 36 mph westbound. The measured 85<sup>th</sup> percentile vehicle travel speed, or the speed at which 85 percent of the observed vehicles traveled at or below, was found to be 37 mph in the eastbound direction and 41 mph westbound, which is 7 to 11 mph *above* the posted speed limit in the vicinity of the Project site (30 mph). The 85<sup>th</sup> percentile speed is used as the basis of engineering design and in the evaluation of sight distances and is often used in establishing posted speed limits.

### **Motor Vehicle Crash Data**

Motor vehicle crash information for the study area was provided by the MassDOT Highway Division Safety Management/Traffic Operations Unit for the most recent five-year period available (2016 through 2020, inclusive) in order to examine motor vehicle crash trends occurring within the study area. The data is summarized by intersection, type, severity, roadway and weather conditions, and day of occurrence, and presented in Table 4.

**Table 4**  
**MOTOR VEHICLE CRASH DATA SUMMARY<sup>a</sup>**

Route 113 in the vicinity of the Project Site Driveway	
Traffic Control Type <sup>b</sup>	U
<i>Year:</i>	
2016	0
2017	0
2018	0
2019	0
<u>2020</u>	<u>1</u>
Total	1
Average	0.2
Crash Rate <sup>c</sup>	0.04
MassDOT Crash Rate <sup>d</sup>	0.57/0.57
Significant? <sup>e</sup>	No
<i>Type:</i>	
Angle	0
Head-On	0
Rear-End	0
Sideswipe	0
Fixed Object	1
Pedestrian/Bicycle	0
<u>Unknown/Other</u>	<u>0</u>
Total	1
<i>Conditions:</i>	
Clear	1
Cloudy	0
Rain	0
Snow/Ice	0
<u>Fog/Smoke</u>	<u>0</u>
Total	1
<i>Lighting:</i>	
Daylight	1
Dawn/Dusk	0
Dark (Road Lit)	0
<u>Dark (Road Unlit)</u>	<u>0</u>
Total	1
<i>Day of Week:</i>	
Monday-Friday	1
Saturday	0
<u>Sunday</u>	<u>0</u>
Total	1
<i>Severity:</i>	
Property Damage Only	1
Non-fatal Injury	0
Fatalities	0
<u>Not Reported</u>	<u>0</u>
Total	1

<sup>a</sup>Source: MassDOT Safety Management/Traffic Operations Unit records, 2016 through 2020.

<sup>b</sup>Traffic Control Type: U = unsignalized.

<sup>c</sup>Crash rate per million vehicles entering the intersection.

<sup>d</sup>Statewide/District crash rate.

<sup>e</sup>The intersection crash rate is significant if it is found to exceed the MassDOT crash rate for the MassDOT Highway Division District in which the Project is located (District 4).

As can be seen in Table 4, Route 113 in the vicinity of the Project site was shown to have one (1) reported motor vehicle crash over the five-year review period, with the Route 113/Project site driveway (exiting) intersection found to have motor vehicle crash rate *below* both the MassDOT statewide and District average crash rates for similar intersections for the MassDOT Highway Division District in which the intersections are located (District 4). The crash was reported to have occurred on a weekday, under clear weather conditions, during daytime, and was identified as a single-vehicle crash with a fixed roadside object that resulted in property damage only.

A review of the MassDOT statewide High Crash Location List indicates that there are no locations within the study area that are included on MassDOT's Highway Safety Improvement Program (HSIP) listing as a high crash cluster location. In addition, no fatal motor vehicle crashes were reported to have occurred at the study area intersections over the five-year review period.

The detailed MassDOT Crash Rate Worksheets and High Crash Location mapping are provided in the Appendix.

## **FUTURE CONDITIONS**

Traffic volumes in the study area were projected to the year 2030, which reflects a seven-year planning horizon consistent with MassDOT guidelines. Independent of the Project, traffic volumes on the roadway network in the year 2030 under No-Build conditions include all existing traffic and new traffic resulting from background traffic growth. Anticipated Project-generated traffic volumes superimposed upon the 2030 No-Build traffic volumes reflect 2030 Build traffic-volume conditions with the Project.

### **Future Traffic Growth**

Future traffic growth is a function of the expected land development in the immediate area and the surrounding region. Several methods can be used to estimate this growth. A procedure frequently employed estimates an annual percentage increase in traffic growth and applies that percentage to all traffic volumes under study. The drawback to such a procedure is that some turning volumes may actually grow at either a higher or a lower rate at particular intersections.

An alternative procedure identifies the location and type of planned development, estimates the traffic to be generated, and assigns it to the area roadway network. This procedure produces a more realistic estimate of growth for local traffic; however, potential population growth and development external to the study area would not be accounted for in the resulting traffic projections.

To provide a conservative analysis framework, both procedures were used, the salient components of which are described below.

### **Specific Development by Others**

The City of Methuen Planning Division of the Department of Economic and Community Development was contacted in order to determine if there were any projects planned within the study area that would have an impact on future traffic volumes at the study intersections. At this time, information was not provided concerning specific development projects by others to be included in this assessment (if any). To the extent that the City identifies specific projects that would result in an increase in traffic within the study area that would exceed the general traffic growth rate (discussion follows), a supplement to this assessment will be prepared.

## **General Background Traffic Growth**

Traffic-volume data compiled by MassDOT for the City of Methuen were reviewed in order to determine general traffic growth trends in the area. This data indicates that annual traffic volumes have fluctuated over the past several years, with the average growth rate found to be approximately 0.63 percent per year. In order to provide a conservative (high) analysis scenario and a prudent planning assessment for the Project, a higher 1.0 percent per year compounded annual background traffic growth rate was used to account for future traffic growth and presently unforeseen development within the study area.

## **Roadway Improvement Projects**

The City of Methuen was contacted and the MassDOT Project Viewer website was reviewed in order to determine if there were any planned future roadway improvement projects expected to be completed within the study area by 2030. Based on this review, no roadway improvement projects aside from routine maintenance activities were identified to be planned within the study area at this time.

## **No-Build Traffic Volumes**

The 2030 No-Build condition peak-hour traffic volumes were developed by applying the 1.0 percent per year compounded annual background traffic growth rate to the 2023 Existing peak-hour traffic volumes. The resulting 2030 No-Build weekday morning, weekday evening, and Saturday midday peak-hour traffic volumes are shown on Figure 3.

## **Project-Generated Traffic**

Design year (2030 Build) traffic volumes for the study area roadways were determined by estimating Project-generated traffic volumes and assigning those volumes on the study roadways. The following sections describe the methodology used to develop the anticipated traffic characteristics of the Project.

As proposed, the Project will entail the construction of a 1,500 sf, single-tunnel, car wash. In order to develop the traffic characteristics of the Project, trip-generation statistics published by the ITE for similar land use as that proposed were used. ITE Land Use Code (LUC) 948, *Automated Car Wash*, was used to develop the traffic characteristics of the Project, the results of which are summarized in Table 5.

**Table 5**  
**TRIP GENERATION SUMMARY**

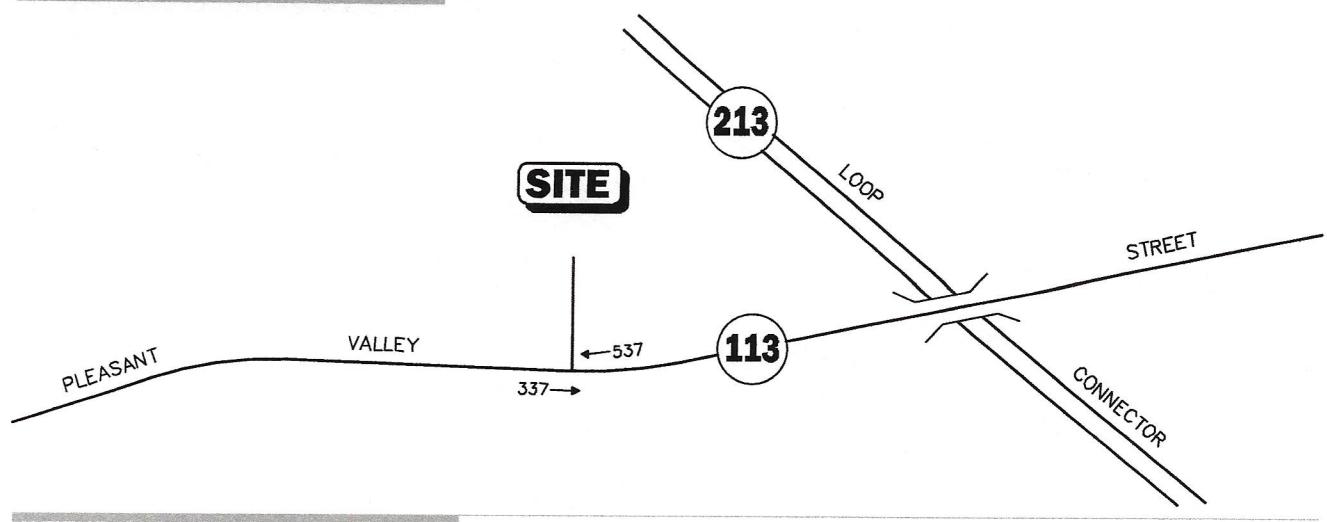
Time Period	Vehicle Trips		
	Entering	Exiting	Total
Average Weekday: <sup>a</sup>	208	208	416
Weekday Morning Peak Hour: <sup>b</sup>	16	15	31
Weekday Evening Peak Hour: <sup>c</sup>	11	10	21
Saturday Midday Peak Hour: <sup>c</sup>	23	23	46

<sup>a</sup>Based on the ratio of the average weekday trip rate to the weekday evening peak-hour trip rate for ITE LUC 947, *Self-Service Car Wash*, applied to the weekday evening peak-hour trip rate.

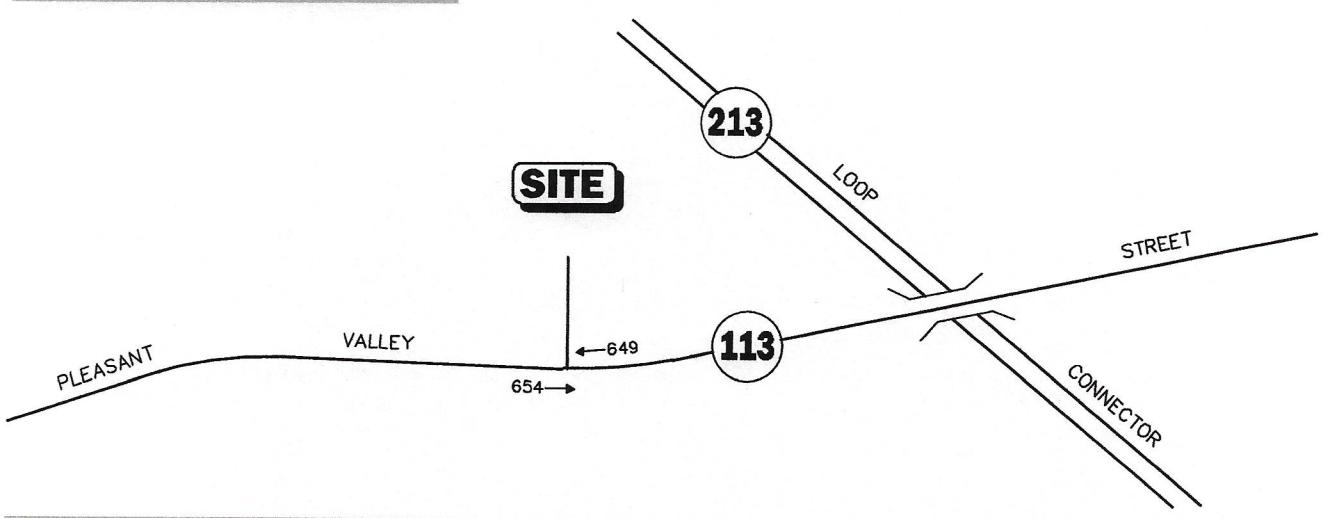
<sup>b</sup>Based on the hourly distribution of entering and exiting vehicle trips by land use for ITE LUC 947, *Self-Service Car Wash*.

<sup>c</sup>Based on ITE LUC 948, *Automated Car Wash*.

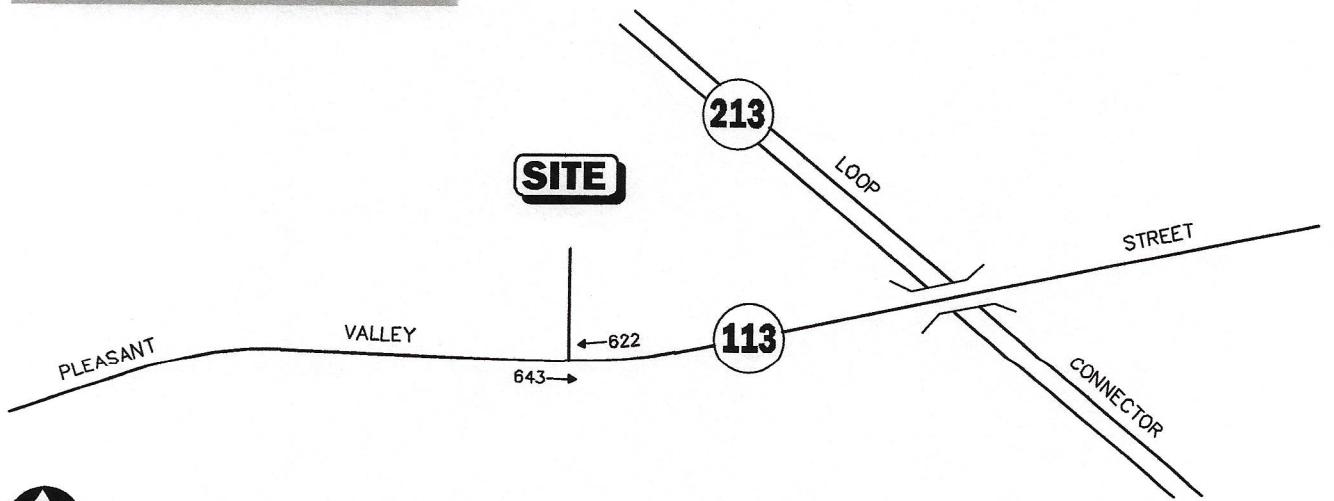
WEEKDAY MORNING PEAK HOUR



WEEKDAY EVENING PEAK HOUR



SATURDAY MIDDAY PEAK HOUR



Not To Scale



Figure 3

2030 No-Build  
Peak-Hour Traffic Volumes

## **Project-Generated Traffic-Volume Summary**

As can be seen in Table 5, the Project is expected to generate approximately 416 vehicle trips on an average weekday (two-way volume over the operational day of the Project, or 208 vehicles entering and 208 exiting), with 31 vehicle trips (16 vehicles entering and 15 exiting) expected during the weekday morning peak hour, 21 vehicle trips (11 vehicles entering and 10 exiting) expected during the weekday evening peak hour and 46 vehicle trips (23 vehicles entering and 23 exiting) expected during the Saturday midday peak hour.

### **Trip Distribution and Assignment**

The directional distribution of generated trips to and from the Project site was determined based on a review of existing traffic patterns within the study area and then refined based on a review of the regional roadway network. The general trip distribution for the Project is graphically depicted on Figure 4. The additional traffic expected to be generated by the Project was assigned on the study area roadway network as shown on Figure 5 for the weekday morning, weekday evening and Saturday midday peak hours.

### **Build Traffic Volumes**

The 2030 Build condition traffic volumes consist of the 2030 No-Build traffic volumes with the addition of the traffic expected to be generated by the Project. The 2030 Build weekday morning, weekday evening and Saturday midday peak-hour traffic volumes are graphically depicted on Figure 6.

## **TRAFFIC OPERATIONS ANALYSIS**

In order to assess the potential impact of the Project on the roadway network, a detailed traffic operations analysis (motorist delays, vehicle queuing, and level of service) was performed for the study area intersection. Capacity analyses provide an indication of how well transportation facilities serve the traffic demands placed upon them, with vehicle queue analyses providing a secondary measure of the operational characteristics of an intersection or section of roadway under study.

In brief, six levels of service are defined for each type of facility. They are given letter designations ranging from A to F, with LOS "A" representing the best operating conditions and LOS "F" representing congested or constrained operations. An LOS of "E" is representative of a transportation facility that is operating at its design capacity while an LOS of "D" is generally defined as the limit of "acceptable" traffic operations. Since the level of service of a traffic facility is a function of the flows placed upon it, such a facility may operate at a wide range of levels of service depending on the time of day, day of week, or period of the year. The Synchro® intersection capacity analysis software, which is based on the analysis methodologies and procedures presented in the *6<sup>th</sup> Edition Highway Capacity Manual (HCM)*<sup>6</sup> for unsignalized intersections was used to complete the level-of-service and vehicle queue analyses.

### **Analysis Results**

Level-of-service and vehicle queue analysis were conducted for 2023 Existing, 2030 No-Build, and 2030 Build conditions for the intersections within the study area. The results of the intersection capacity and vehicle queue analyses are summarized in Table 6, with the detailed analysis results attached. For the purpose of this analysis, the Project site driveways were analyzed as a single intersection.

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<sup>6</sup> *Highway Capacity Manual*, Transportation Research Board; Washington, DC; 2016.

Legend:

XX Entering Trips  
(XX) Exiting Trips

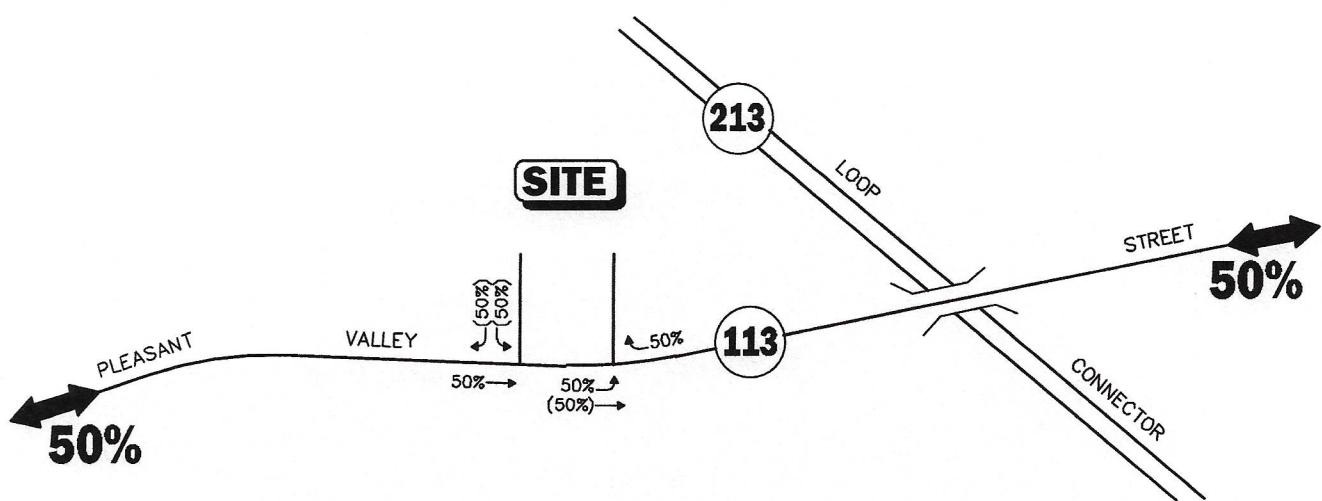


Figure 4

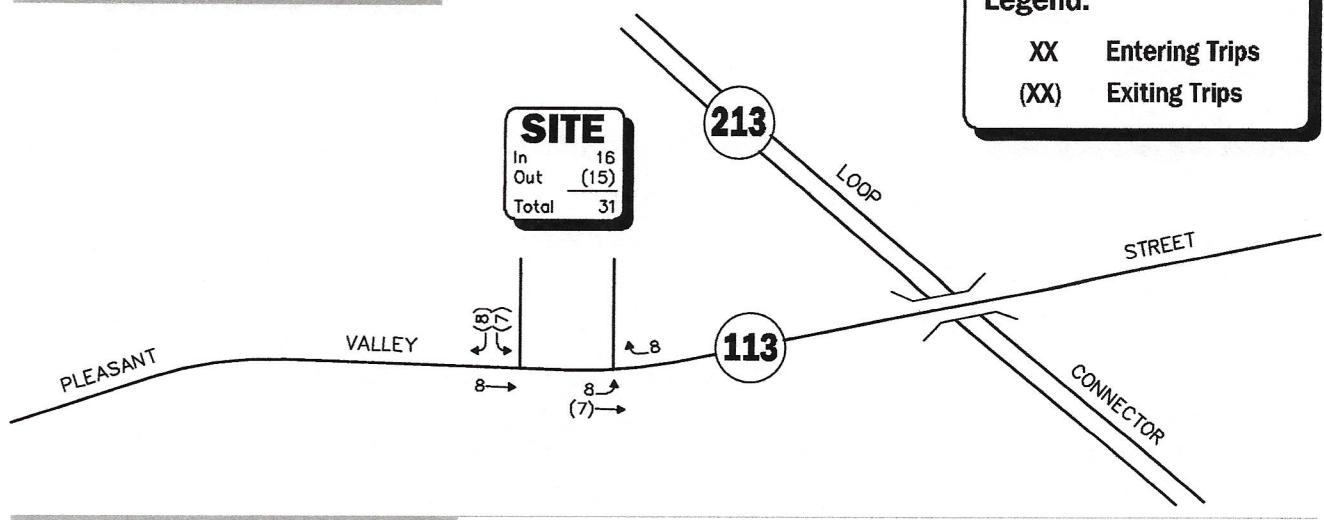
Trip Distribution Map



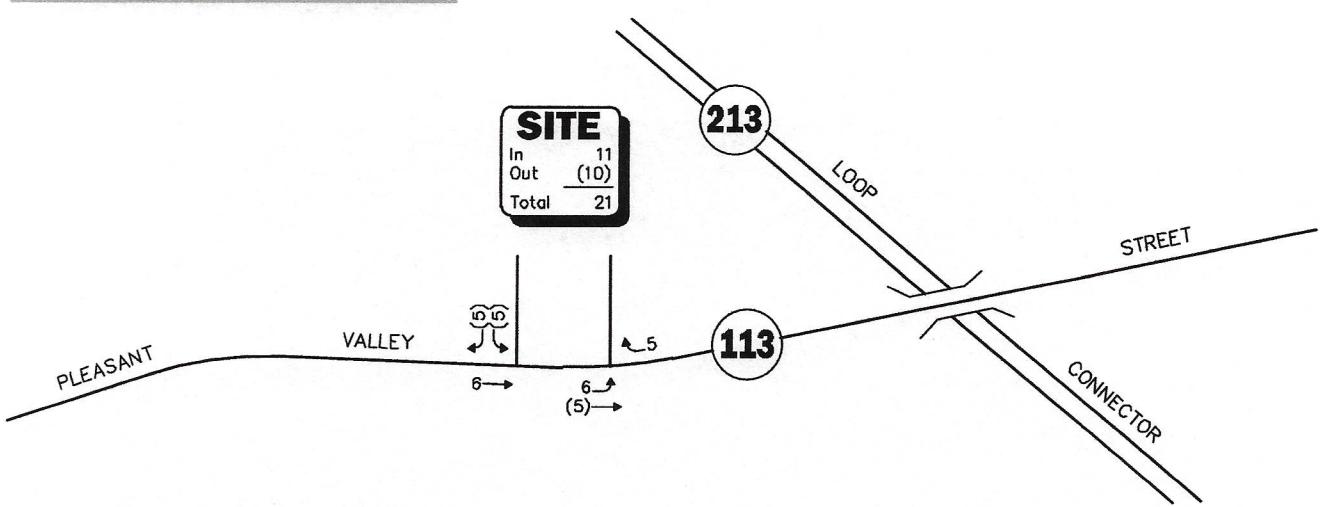
Not To Scale

**VAI** Vanasse &  
Associates inc

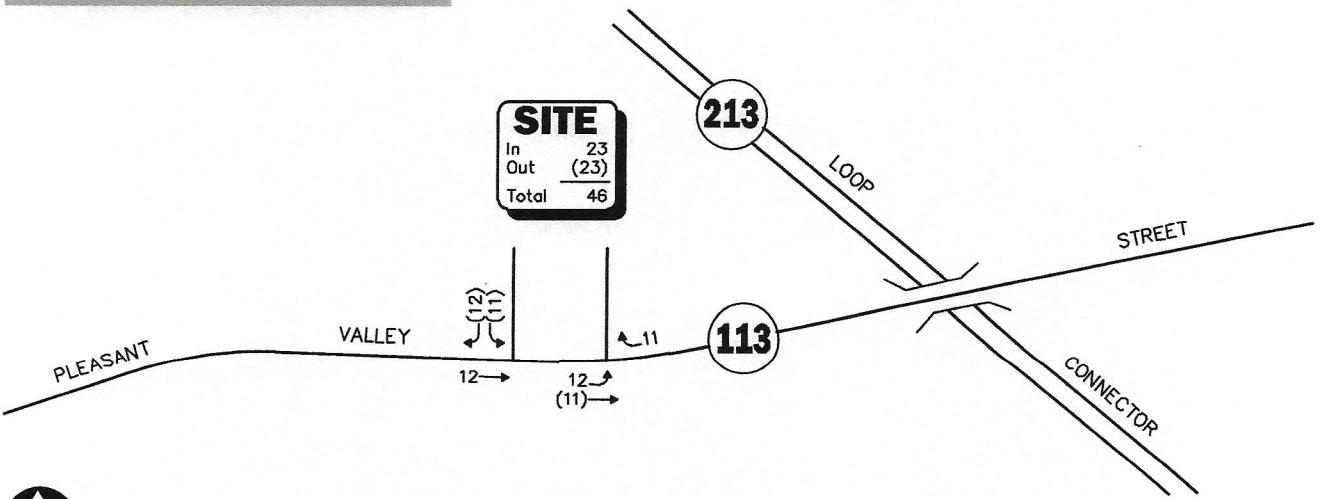
WEEKDAY MORNING PEAK HOUR



WEEKDAY EVENING PEAK HOUR



SATURDAY MIDDAY PEAK HOUR



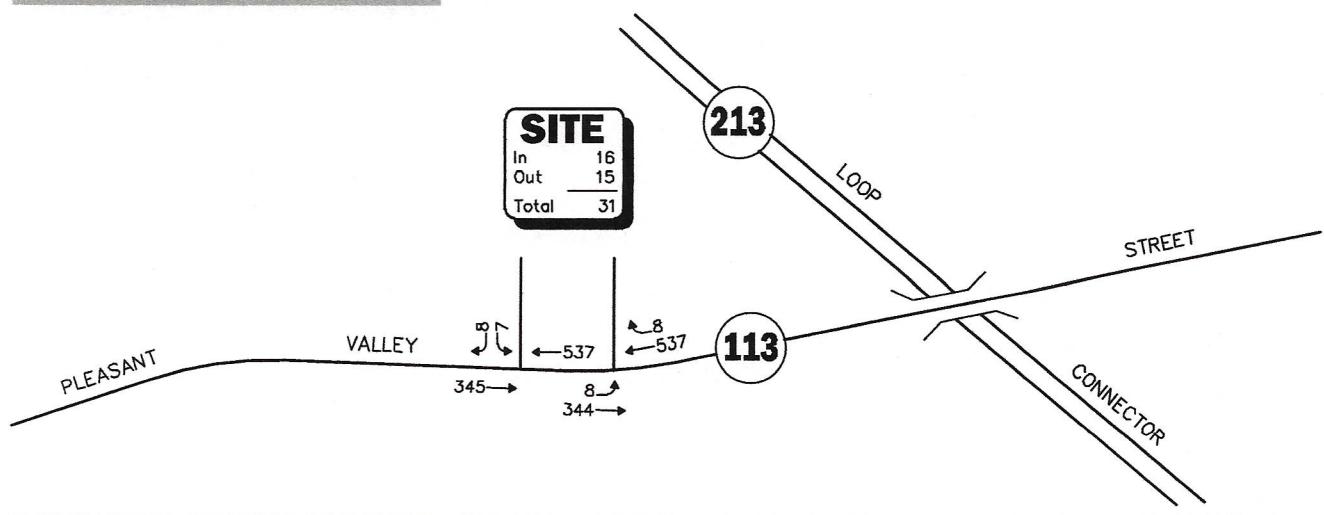
Not To Scale



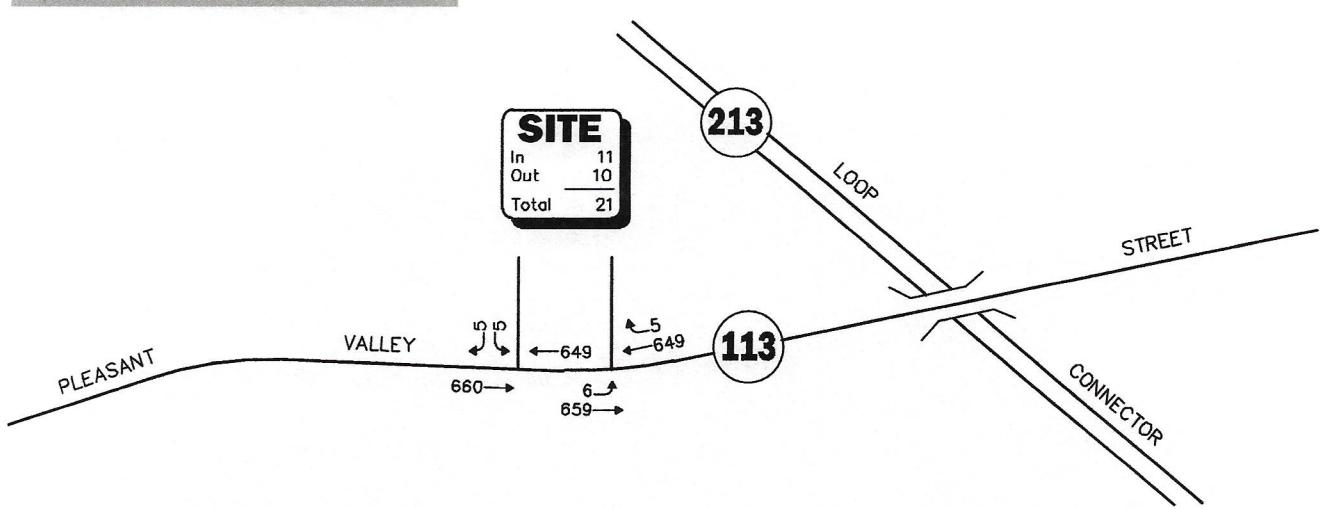
Figure 5

Project-Generated  
Peak-Hour Traffic Volumes

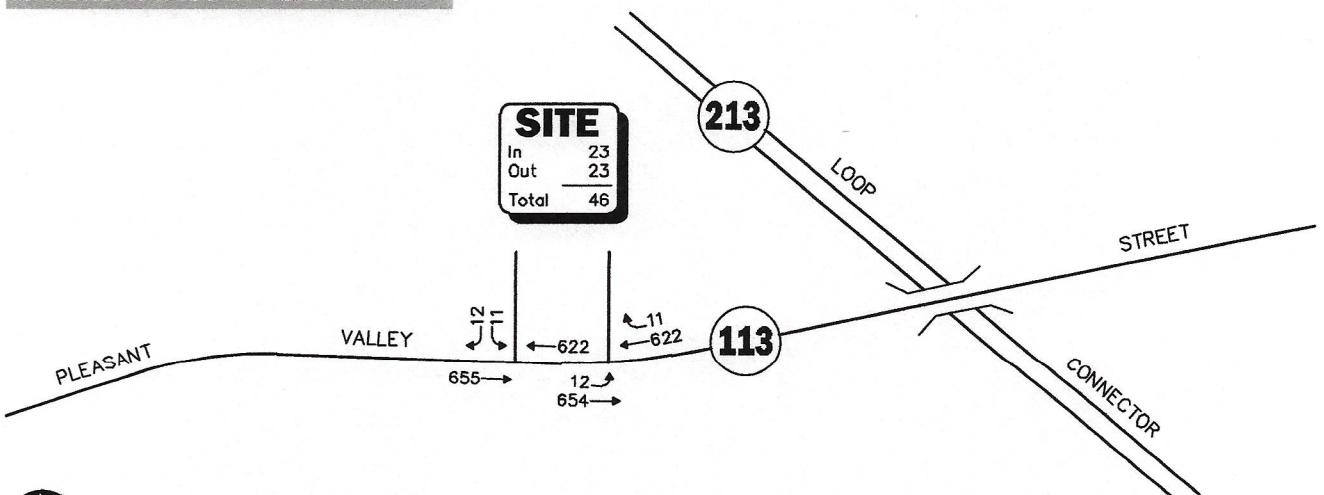
WEEKDAY MORNING PEAK HOUR



WEEKDAY EVENING PEAK HOUR



SATURDAY MIDDAY PEAK HOUR



Not To Scale



Figure 6

2030 Build  
Peak-Hour Traffic Volumes

The following is a summary of the level-of-service and vehicle queue analyses for intersections within the study area. For context, we note that an LOS of “D” or better is generally defined as “acceptable” operating conditions.

#### **Route 113 at the Project Site Driveway**

All movements exiting the Project site are predicted to operate at LOS C during the peak hours, with vehicle queues of up to one (1) vehicle predicted. All movements along Route 113 approaching the driveway were shown to operate at LOS A during the peak hours with no (0) residual vehicle queuing.

**Table 6**  
**UNSIGNALIZED INTERSECTION LEVEL-OF-SERVICE AND VEHICLE QUEUE SUMMARY**

Unsignaled Intersection/Peak-Hour/Movement	2023 Existing				2030 No-Build				2030 Build			
	Demand <sup>a</sup>	Delay <sup>b</sup>	LOS <sup>c</sup>	Queue <sup>d</sup> 95 <sup>th</sup>	Demand	Delay	LOS	Queue 95 <sup>th</sup>	Demand	Delay	LOS	Queue 95 <sup>th</sup>
<i>Route 113 at the Project Site Driveway</i>												
<i>Weekday Morning:</i>												
Route 113 EB LT/TH	--	--	--	--	--	--	--	--	345	0.2	A	0
Route 113 WB TH/RT	--	--	--	--	--	--	--	--	545	0.0	A	0
Project Site Driveway SB LT/RT	--	--	--	--	--	--	--	--	15	16.1	C	0
<i>Weekday Evening:</i>												
Project Site Driveway EB LT/TH	--	--	--	--	--	--	--	--	660	0.1	A	0
Route 113 NB LT/TH	--	--	--	--	--	--	--	--	654	0.0	A	0
Project Site Driveway SB LT/RT	--	--	--	--	--	--	--	--	10	22.0	C	0
<i>Saturday Midday:</i>												
Route 113 EB LT/TH	--	--	--	--	--	--	--	--	655	0.2	A	0
Route 113 WB TH/RT	--	--	--	--	--	--	--	--	633	0.0	A	0
Project Site Driveway SB LT/RT	--	--	--	--	--	--	--	--	23	22.2	C	1

<sup>a</sup>Demand in vehicles per hour.

<sup>b</sup>Average control delay per vehicle (in seconds).

<sup>c</sup>Level of service.

<sup>d</sup>Queue length in vehicles.

EB = eastbound; SB = southbound; WB = westbound; LT = left-turning movements; TH = through movements; RT = right-turning movements.

## **SIGHT DISTANCE ASSESSMENT**

Sight distance measurements were performed at the intersections of the Project site driveways with Route 113 in accordance with MassDOT and American Association of State Highway and Transportation Officials (AASHTO)<sup>7</sup> requirements. Both stopping sight distance (SSD) and intersection sight distance (ISD) measurements were performed. In brief, SSD is the distance required by a vehicle traveling at the design speed of a roadway, on wet pavement, to stop prior to striking an object in its travel path. ISD or corner sight distance (CSD) is the sight distance required by a driver entering or crossing an intersecting roadway to perceive an oncoming vehicle and safely complete a turning or crossing maneuver with oncoming traffic. In accordance with AASHTO standards, if the measured ISD is at least equal to the required SSD value for the appropriate design speed, the intersection can operate in a safe manner. Table 7 presents the measured SSD and ISD at the subject intersections.

**Table 7**  
**SIGHT DISTANCE MEASUREMENTS<sup>a</sup>**

Intersection/Sight Distance Measurement	Feet		
	Required Minimum (SSD)	Desirable (ISD) <sup>b</sup>	Measured
<b>Route 113 at the Project Site Entrance Driveway</b>			
<i>Stopping Sight Distance:</i>			
Route 113 approaching from the east	360	--	500+
Route 113 approaching from the west	360	--	500+
<b>Route 113 at the Project Site Exit Driveway</b>			
<i>Stopping Sight Distance:</i>			
Route 113 approaching from the east	360	--	500+
Route 113 approaching from the west	360	--	500+
<i>Intersection Sight Distance:</i>			
Looking to the east from the Project Site Driveway	360	500	500+
Looking to the west from the Project Site Driveway	360	430	202/400 <sup>c</sup>

<sup>a</sup>Recommended minimum values obtained from *A Policy on Geometric Design of Highways and Streets*, 7<sup>th</sup> Edition; American Association of State Highway and Transportation Officials (AASHTO); 2018; and based on a 45 mph approach speed on Route 113.

<sup>b</sup>Values shown are the intersection sight distance for a vehicle turning right or left exiting a roadway under STOP control such that motorists approaching the intersection on the major street should not need to adjust their travel speed to less than 70 percent of their initial approach speed.

<sup>c</sup>Available sight distance with the selective trimming/removal of vegetation located within the sight triangle areas.

As can be seen in Table 7, with the selective trimming/removal of vegetation located within the sight triangle areas of Project site exit driveway, the available lines of sight to and from the Project site driveway intersections with Route 113 will exceed the recommended minimum sight distance to function in a safe (SSD) and efficient (ISD) manner based on a 45 mph approach speed, which is above the measured 85<sup>th</sup> percentile vehicle travel speed (37/41 mph) in the vicinity of the Project site and the posted speed limit (30 mph).

<sup>7</sup> *A Policy on Geometric Design of Highway and Streets*, 7<sup>th</sup> Edition; American Association of State Highway and Transportation Officials (AASHTO); Washington D.C.; 2018.

## **SUMMARY**

VAI has completed a detailed assessment of the potential impacts on the transportation infrastructure associated with the proposed construction of an automated car wash to be located at 128 Pleasant Valley Street (Route 113) in Methuen, Massachusetts. The following specific areas have been evaluated as they relate to the Project: i) access requirements; ii) potential off-site improvements; and iii) safety considerations; under existing and future conditions, both with and without the Project. Based on this assessment, we have concluded the following with respect to the Project:

1. Using trip-generation statistics published by the ITE,<sup>8</sup> the Project is expected to generate approximately 416 vehicle trips on an average weekday (two-way volume over the operational day of the Project), with 31 vehicle trips expected during the weekday morning peak hour, 21 vehicle trips expected during the weekday evening peak hour, and 46 vehicle trips expected during the Saturday midday peak hour;
2. The Project will not result in a significant impact (increase) on motorist delays or vehicle queuing over Existing or anticipated future conditions without the Project (No-Build conditions), with all movements along Route 113 approaching the Project site driveway shown to continue to operate at LOS A with negligible vehicle queuing;
3. All movements exiting the Project site driveway to Route 113 are predicted to operate at LOS C during the peak hours with vehicle queues of up to one (1) vehicle predicted;
4. No apparent safety deficiencies were noted with respect to the motor vehicle crash history in the vicinity of the Project site; and
5. Lines of sight at the intersections of the Project site driveways with Route 113 were found to exceed or can be made to exceed the recommended minimum distance for the intersections to operate in a safe and efficient manner based on the appropriate approach speed.

In consideration of the above, we have concluded that the Project can be accommodated within the confines of the existing transportation infrastructure in a safe and efficient manner with the implementation of the recommendations that follow.

## **RECOMMENDATIONS**

A detailed transportation improvement program has been developed that is designed to provide safe and efficient access to the Project site and address any deficiencies identified as a part of this assessment. The following improvements have been recommended as a part of this evaluation and, where applicable, will be completed in conjunction with the Project subject to receipt of all necessary rights, permits, and approvals.

### **Project Access**

Access to the Project site will be provided by way of two driveways that intersect the north side of Route 113 along the property frontage. The eastern driveway will be restricted to entering movements only, with the western driveway restricted to exiting movements only. The following recommendations are offered with respect to the design and operation of the Project site access and internal circulation:

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<sup>8</sup>Institute of Transportation Engineers, op. cit. 1.

- The Project site driveways should be a minimum of 20 feet in width, unless a reduced width is approved by the Methuen Fire Department, and designed to accommodate the turning and maneuvering requirements of the largest anticipated responding emergency vehicle.
- The dimensions of the parallel parking spaces should be 8-feet and 22-feet long.
- A vehicle queue by-pass lane should be provided around the car wash and a re-circulation lane should be developed at the front of the car wash that does not require vehicles to use Route 113 to re-enter the car wash.
- Vehicles exiting the Project site should be placed under STOP-sign control with a marked STOP-line provided.
- All signs and pavement markings to be installed within the Project site should conform to the applicable standards of the *Manual on Uniform Traffic Control Devices* (MUTCD).<sup>9</sup>
- “ONE WAY” and “DO NOT ENTER” signs should be installed at the Project site driveways and within the Project site to regulate the one-way circulation pattern and to define the entrance and exit driveways.
- Signs and landscaping to be installed as a part of the Project within the intersection sight triangle areas of the Project site driveways should be designed and maintained so as not to restrict lines of sight.
- Existing vegetation located within the sight triangle areas of the Project site driveways should be selectively trimmed or removed and maintained so as to provide the necessary sightlines for the driveways to operate in a safe manner.
- Snow accumulations (windrows) within sight triangle areas should be promptly removed where such accumulations would impede sightlines.
- A peak season operations plan should be developed that includes on-site staffing to manage vehicle queuing.

With implementation of the aforementioned recommendations, safe and efficient access will be provided to the Project site and the Project can be accommodated within the confines of the existing transportation system.

cc: File

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<sup>9</sup>*Manual on Uniform Traffic Control Devices (MUTCD)*; Federal Highway Administration; Washington, D.C.; 2009.

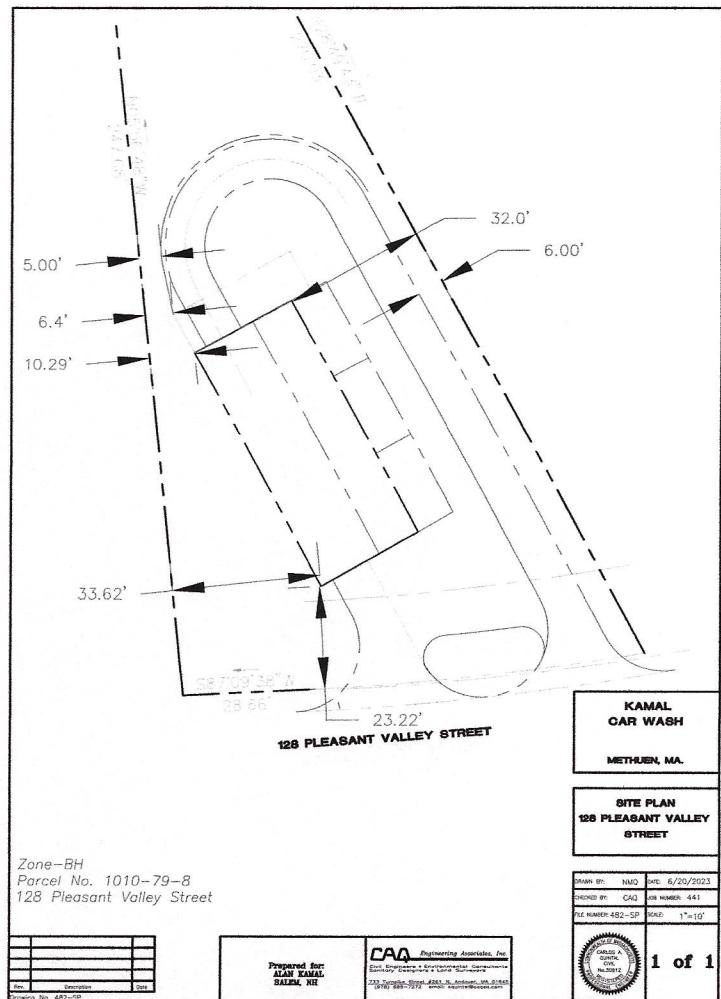
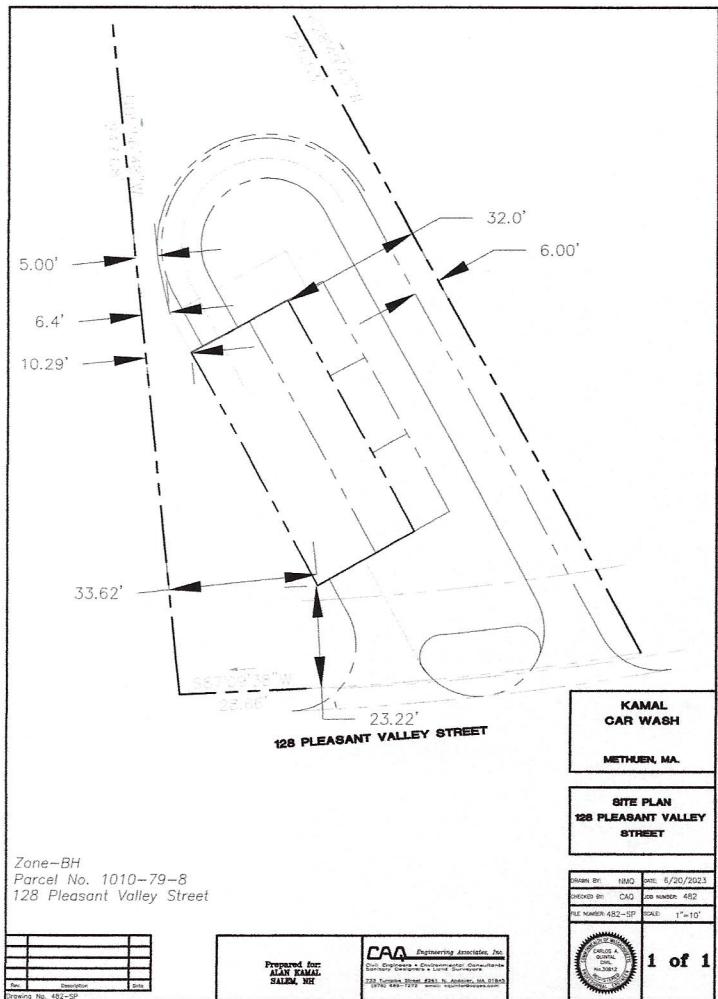
## ATTACHMENTS

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PROJECT SITE PLAN  
AUTOMATIC TRAFFIC RECORDER COUNT DATA  
SEASONAL ADJUSTMENT DATA  
PUBLIC TRANSPORTATION INFORMATION  
VEHICLE TRAVEL SPEED DATA  
MASSDOT CRASH RATE WORKSHEET AND HIGH CRASH LOCATION MAPPING  
GENERAL BACKGROUND TRAFFIC GROWTH  
TRIP-GENERATION CALCULATIONS  
CAPACITY ANALYSIS WORKSHEETS

**PROJECT SITE PLAN**

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AUTOMATIC TRAFFIC RECORDER COUNT DATA

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA

Site Code: 98290001

9/21/2023	EB		Hour Totals		WB		Hour Totals		Combined Totals		
	Time	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon
12:00		7	90			7	122				
12:15		8	98			7	117				
12:30		10	109			5	95				
12:45		6	109	31	406	3	103	22	437	53	843
1:00		1	104			4	118				
1:15		5	90			8	108				
1:30		3	123			4	124				
1:45		4	121	13	438	2	116	18	466	31	904
2:00		1	113			1	109				
2:15		0	132			1	104				
2:30		4	127			3	111				
2:45		3	128	8	500	3	110	8	434	16	934
3:00		5	156			3	111				
3:15		0	136			10	112				
3:30		4	151			3	121				
3:45		2	140	11	583	2	148	18	492	29	1075
4:00		4	159			7	131				
4:15		3	125			13	145				
4:30		8	163			9	157				
4:45		13	137	28	584	23	152	52	585	80	1169
5:00		11	139			35	142				
5:15		16	171			28	154				
5:30		15	147			32	134				
5:45		17	179	59	636	40	128	135	558	194	1194
6:00		30	132			40	118				
6:15		37	154			48	120				
6:30		39	112			98	100				
6:45		51	124	157	522	124	109	310	447	467	969
7:00		52	105			106	89				
7:15		55	97			119	61				
7:30		74	85			136	58				
7:45		97	94	278	381	112	63	473	271	751	652
8:00		79	81			140	59				
8:15		64	83			113	72				
8:30		100	64			109	61				
8:45		112	54	355	282	80	43	442	235	797	517
9:00		85	62			95	41				
9:15		65	68			96	38				
9:30		89	47			84	28				
9:45		94	43	333	220	93	22	368	129	701	349
10:00		77	44			90	26				
10:15		94	43			91	25				
10:30		86	17			108	14				
10:45		125	23	382	127	95	20	384	85	766	212
11:00		83	20			115	9				
11:15		84	20			126	16				
11:30		91	19			120	7				
11:45		109	7	367	66	123	6	484	38	851	104
Total		2022	4745			2714	4177			4736	8922
Percent		29.9%	70.1%			39.4%	60.6%			34.7%	65.3%

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA

Site Code: 98290001

9/22/2023	EB		Hour Totals		WB		Hour Totals		Combined Totals		
	Time	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon
12:00		9	121			6	116				
12:15		13	119			8	111				
12:30		12	119			2	124				
12:45		6	126	40	485	4	112	20	463	60	948
1:00		10	109			3	118				
1:15		4	117			4	103				
1:30		2	114			4	98				
1:45		7	113	23	453	2	130	13	449	36	902
2:00		6	161			4	123				
2:15		2	143			5	145				
2:30		2	149			3	140				
2:45		2	167	12	620	1	132	13	540	25	1160
3:00		3	192			4	125				
3:15		5	200			8	131				
3:30		3	190			2	124				
3:45		4	159	15	741	7	129	21	509	36	1250
4:00		8	171			6	129				
4:15		10	179			16	146				
4:30		7	177			15	149				
4:45		6	158	31	685	22	171	59	595	90	1280
5:00		12	159			25	160				
5:15		18	141			24	140				
5:30		19	118			39	130				
5:45		23	143	72	561	40	125	128	555	200	1116
6:00		27	151			35	130				
6:15		34	140			49	120				
6:30		29	130			86	101				
6:45		49	108	139	529	114	108	284	459	423	988
7:00		61	115			87	86				
7:15		50	107			118	82				
7:30		67	108			110	67				
7:45		105	86	283	416	116	51	431	286	714	702
8:00		84	73			123	59				
8:15		91	73			113	57				
8:30		92	70			104	45				
8:45		125	64	392	280	100	52	440	213	832	493
9:00		76	64			103	51				
9:15		92	56			92	39				
9:30		98	39			92	32				
9:45		106	36	372	195	97	36	384	158	756	353
10:00		93	46			78	28				
10:15		73	44			119	32				
10:30		90	36			101	25				
10:45		93	32	349	158	96	26	394	111	743	269
11:00		115	27			92	19				
11:15		100	27			110	23				
11:30		99	12			114	13				
11:45		105	17	419	83	113	8	429	63	848	146
Total		2147	5206			2616	4401			4763	9607
Percent		29.2%	70.8%			37.3%	62.7%			33.1%	66.9%
Grand Total		4169	9951			5330	8578			9499	18529
Percent		29.5%	70.5%			38.3%	61.7%			33.9%	66.1%
ADT		ADT: 14,014		AADT: 14,014							

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA

Site Code: 98290001

9/18/2023	Monday		Tuesday		Wednesday		Thursday		Friday		Saturday		Sunday		Week Average	
Time	EB	WB	EB	WB	EB	WB	EB	WB	EB	WB	EB	WB	EB	WB	EB	WB
12:00 AM	*	*	*	*	*	*	31	22	40	20	*	*	*	*	36	21
1:00	*	*	*	*	*	*	13	18	23	13	*	*	*	*	18	16
2:00	*	*	*	*	*	*	8	8	12	13	*	*	*	*	10	10
3:00	*	*	*	*	*	*	11	18	15	21	*	*	*	*	13	20
4:00	*	*	*	*	*	*	28	52	31	59	*	*	*	*	30	56
5:00	*	*	*	*	*	*	59	135	72	128	*	*	*	*	66	132
6:00	*	*	*	*	*	*	157	310	139	284	*	*	*	*	148	297
7:00	*	*	*	*	*	*	278	473	283	431	*	*	*	*	280	452
8:00	*	*	*	*	*	*	355	442	392	440	*	*	*	*	374	441
9:00	*	*	*	*	*	*	333	368	372	384	*	*	*	*	352	376
10:00	*	*	*	*	*	*	382	384	349	394	*	*	*	*	366	389
11:00	*	*	*	*	*	*	367	484	419	429	*	*	*	*	393	456
12:00 PM	*	*	*	*	*	*	406	437	485	463	*	*	*	*	446	450
1:00	*	*	*	*	*	*	438	466	453	449	*	*	*	*	446	458
2:00	*	*	*	*	*	*	500	434	620	540	*	*	*	*	560	487
3:00	*	*	*	*	*	*	583	492	741	509	*	*	*	*	662	500
4:00	*	*	*	*	*	*	584	585	685	595	*	*	*	*	634	590
5:00	*	*	*	*	*	*	636	558	561	555	*	*	*	*	598	556
6:00	*	*	*	*	*	*	522	447	529	459	*	*	*	*	526	453
7:00	*	*	*	*	*	*	381	271	416	286	*	*	*	*	398	278
8:00	*	*	*	*	*	*	282	235	280	213	*	*	*	*	281	224
9:00	*	*	*	*	*	*	220	129	195	158	*	*	*	*	208	144
10:00	*	*	*	*	*	*	127	85	158	111	*	*	*	*	142	98
11:00	*	*	*	*	*	*	66	38	27	19	*	*	*	*	46	28
Total Day	0	0	0	0	0	0	6767	6891	7297	6973	0	0	0	0	7033	6932
AM Peak Volume							10:00	11:00	11:00	8:00					11:00	11:00
PM Peak Volume							382	484	419	440					393	456
Comb Total ADT	0	0	0	0	0	0	13658	14270	0	0	0	0	0	0	13965	
	ADT: 14,014		AADT: 14,014													

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA

Site Code: 982900S1

9/30/2023	EB		Hour Totals		WB		Hour Totals		Combined Totals		
	Time	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon	Morning	Afternoon
12:00		7	137			11	159				
12:15		12	146			13	149				
12:30		14	132			11	139				
12:45		14	164	47	579	11	153	46	600	93	1179
1:00		8	158			11	139				
1:15		7	139			6	112				
1:30		6	132			4	133				
1:45		9	127	30	556	8	108	29	492	59	1048
2:00		3	143			4	108				
2:15		7	124			3	128				
2:30		7	131			4	114				
2:45		2	116	19	514	4	117	15	467	34	981
3:00		1	143			4	107				
3:15		5	112			3	86				
3:30		6	129			4	130				
3:45		2	122	14	506	2	110	13	433	27	939
4:00		1	129			2	114				
4:15		10	103			9	114				
4:30		0	117			7	116				
4:45		4	123	15	472	8	112	26	456	41	928
5:00		9	115			7	107				
5:15		2	141			8	107				
5:30		4	107			10	106				
5:45		11	109	26	472	9	92	34	412	60	884
6:00		7	113			7	91				
6:15		12	97			17	109				
6:30		10	94			21	93				
6:45		24	113	53	417	50	82	95	375	148	792
7:00		27	96			43	62				
7:15		28	73			37	59				
7:30		42	55			51	60				
7:45		41	60	138	284	48	67	179	248	317	532
8:00		42	86			53	72				
8:15		50	64			73	46				
8:30		50	67			81	40				
8:45		78	67	220	284	90	44	297	202	517	486
9:00		65	48			90	37				
9:15		78	59			105	33				
9:30		83	67			103	31				
9:45		105	44	331	218	124	28	422	129	753	347
10:00		104	32			128	28				
10:15		125	37			129	33				
10:30		111	33			125	27				
10:45		132	34	472	136	129	15	511	103	983	239
11:00		95	34			139	25				
11:15		106	28			161	31				
11:30		130	20			139	10				
11:45		128	20	459	102	133	15	572	81	1031	183
Total		1824	4540			2239	3998			4063	8538
Percent		28.7%	71.3%			35.9%	64.1%			32.2%	67.8%
Grand Total		1824	4540			2239	3998			4063	8538
Percent		28.7%	71.3%			35.9%	64.1%			32.2%	67.8%
ADT		ADT: 12,601		AADT: 12,601							

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA

Site Code: 982900S1

9/30/2023	EB	WB	
Time			Total
12:00 AM	47	46	93
1:00	30	29	59
2:00	19	15	34
3:00	14	13	27
4:00	15	26	41
5:00	26	34	60
6:00	53	95	148
7:00	138	179	317
8:00	220	297	517
9:00	331	422	753
10:00	472	511	983
11:00	459	572	1031
12:00 PM	579	600	1179
1:00	556	492	1048
2:00	514	467	981
3:00	506	433	939
4:00	472	456	928
5:00	472	412	884
6:00	417	375	792
7:00	284	248	532
8:00	284	202	486
9:00	218	129	347
10:00	136	103	239
11:00	34	25	59
Total	6296	6181	12477
Percent	50.5%	49.5%	
AM Peak	10:00	11:00	11:00
Volume	472	572	1031
PM Peak	12:00 PM	12:00 PM	12:00 PM
Volume	579	600	1179
Grand Total	6296	6181	12477
Percent	50.5%	49.5%	
ADT	ADT: 12,601		AADT: 12,601

**SEASONAL ADJUSTMENT DATA**

Massachusetts Highway Department  
 Statewide Traffic Data Collection  
 2019 Weekday Seasonal Factors

Factor Group	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	Axle Factor
R1	1.22	1.14	1.12	1.06	1.00	0.96	0.87	0.85	0.96	0.99	1.04	1.12	0.85
R2	0.95	0.96	0.98	0.97	0.97	0.93	0.97	0.94	0.96	0.90	0.92	0.93	0.96
R3	1.15	1.06	1.07	1.00	0.89	0.88	0.89	0.89	0.95	0.92	1.02	1.01	0.97
R4-R7	1.09	1.09	1.11	1.02	0.96	0.92	0.89	0.89	0.99	0.98	1.09	1.13	0.98
U1-Boston	1.03	1.01	0.98	0.94	0.94	0.92	0.95	0.93	0.94	0.94	0.97	1.04	0.96
U1-Essex	1.09	1.06	1.03	0.99	0.94	0.90	0.88	0.86	0.93	0.94	0.99	1.06	0.93
U1-Southeast	1.06	1.05	1.01	0.97	0.95	0.93	0.93	0.90	0.94	0.94	0.98	1.04	0.98
U1-West	1.19	1.14	1.09	0.95	0.92	0.89	0.89	0.86	0.91	0.95	0.97	1.07	0.84
U1-Worcester	1.02	1.04	0.97	0.94	0.93	0.91	0.95	0.91	0.93	0.92	0.95	1.10	0.88
U2	1.01	1.00	0.94	0.93	0.91	0.89	0.93	0.90	0.90	0.91	0.94	1.02	0.99
U3	1.06	1.03	0.98	0.94	0.93	0.91	0.95	0.91	0.92	0.93	0.97	1.00	0.98
U4-U7	1.01	1.00	0.95	0.92	0.88	0.86	0.92	0.91	0.92	0.94	0.99	1.04	0.99
Rec - East	1.04	1.16	1.12	0.98	0.92	0.88	0.77	0.81	0.94	1.02	1.08	1.12	0.99
Rec - West	1.30	1.23	1.32	1.18	0.95	0.82	0.70	0.69	0.97	0.96	1.16	1.15	0.98

Round off:

0-999 = 10

>1000 = 100

U = Urban

R = Rural

- 1 - Interstate
- 2 - Freeway and Expressway
- 3 - Other Principal Arterial
- 4 - Minor Arterial
- 5 - Major Collector
- 6 - Minor Collector
- 7 - Local Road and Street

**Recreational - East Group** - Cape Cod (all towns) including the town of Plymouth south of Route 3A (stations 7014, 7079, 7080, 7090, 7091, 7092, 7093, 7094, 7095, 7096, 7097, 7108 and 7178), Martha's Vineyard and Nantucket.

**Recreational - West Group** - Continuous Stations 2 and 189 including stations

1066, 1067, 1083, 1084, 1085, 1086, 1087, 1088, 1089, 1090, 1091, 1092, 1093, 1094, 1095, 1096, 1097, 1098, 1099, 1100, 1101, 1102, 1103, 1104, 1105, 1106, 1107, 1108, 1113, 1114, 1116, 2196, 2197 and 2198.

PUBLIC TRANSPORTATION INFORMATION

**ROUTE 1 OUTBOUND**  
**Lawrence-Haverhill via The Loop/Pleasant Valley St.**  
**WEEKDAYS**

1	2	3	4	5	6	7	8
Bus starts at Buckley Transportation Center	Bus Leaves from Jackson & Swan	Bus Leaves from The Loop	Bus Leaves from Methuen Plaza Walmart	Bus Leaves from Target Plaza	Bus Leaves from Pleasant Valley & Merrimack	Bus Leaves from Lowell & River	Bus ends at Washington Sq. Transit Station
5:00	5:05	5:20	5:23	5:25	5:30	5:35	5:40
5:30	5:35	5:50	5:53	5:55	6:00	6:05	6:10
6:00	6:05	6:20	6:23	6:25	6:30	6:35	6:40
6:30	6:35	6:50	6:53	6:55	7:00	7:05	7:10
7:00	7:05	7:20	7:23	7:25	7:30	7:35	7:40
7:30	7:35	7:50	7:53	7:55	8:00	8:05	8:10
8:00	8:05	8:20	8:23	8:25	8:30	8:35	8:40
8:30	8:35	8:50	8:53	8:55	9:00	9:05	9:10
9:00	9:05	9:20	9:23	9:25	9:30	9:35	9:40
9:30	9:35	9:50	9:53	9:55	10:00	10:05	10:10
10:00	10:05	10:20	10:23	10:25	10:30	10:35	10:40
10:30	10:35	10:50	10:53	10:55	11:00	11:05	11:10
11:00	11:05	11:20	11:23	11:25	11:30	11:35	11:40
11:30	11:35	11:50	11:53	11:55	12:00	12:05	12:10
12:00	12:05	12:20	12:23	12:25	12:30	12:35	12:40
12:30	12:35	12:50	12:53	12:55	1:00	1:05	1:10
1:00	1:05	1:20	1:23	1:25	1:30	1:35	1:40
1:30	1:35	1:50	1:53	1:55	2:00	2:05	2:10
2:00	2:05	2:20	2:23	2:25	2:30	2:35	2:40
2:30	2:35	2:50	2:53	2:55	3:00	3:05	3:10
3:00	3:05	3:20	3:23	3:25	3:30	3:35	3:40
3:30	3:35	3:50	3:53	3:55	4:00	4:05	4:10
4:00	4:05	4:20	4:23	4:25	4:30	4:35	4:40
4:30	4:35	4:50	4:53	4:55	5:00	5:05	5:10
5:00	5:05	5:20	5:23	5:25	5:30	5:35	5:40
5:30	5:35	5:50	5:53	5:55	6:00	6:05	6:10
6:00	6:05	6:20	6:23	6:25	6:30	6:35	6:40
6:30	6:35	6:50	6:53	6:55	7:00	7:05	7:10
7:00	7:05	7:20	7:23	7:25	7:30	7:35	7:40
8:00	8:05	8:20	8:23	8:25	8:30	8:35	8:40
9:00	9:05	9:20	9:23	9:25	9:30	9:35	9:40

**SATURDAYS**

7:00	7:05	7:20	7:23	7:25	7:30	7:35	7:40
8:00	8:05	8:20	8:23	8:25	8:30	8:35	8:40
9:00	9:05	9:20	9:23	9:25	9:30	9:35	9:40
10:00	10:05	10:20	10:23	10:25	10:30	10:35	10:40
10:30	10:35	10:50	10:53	10:55	11:00	11:05	11:10
11:00	11:05	11:20	11:23	11:25	11:30	11:35	11:40
11:30	11:35	11:50	11:53	11:55	12:00	12:05	12:10
12:00	12:05	12:20	12:23	12:25	12:30	12:35	12:40
12:30	12:35	12:50	12:53	12:55	1:00	1:05	1:10
1:00	1:05	1:20	1:23	1:25	1:30	1:35	1:40
1:30	1:35	1:50	1:53	1:55	2:00	2:05	2:10
2:00	2:05	2:20	2:23	2:25	2:30	2:35	2:40
2:30	2:35	2:50	2:53	2:55	3:00	3:05	3:10
3:00	3:05	3:20	3:23	3:25	3:30	3:35	3:40
3:30	3:35	3:50	3:53	3:55	4:00	4:05	4:10
4:00	4:05	4:20	4:23	4:25	4:30	4:35	4:40
4:30	4:35	4:50	4:53	4:55	5:00	5:05	5:10
5:00	5:05	5:20	5:23	5:25	5:30	5:35	5:40
6:00	6:05	6:20	6:23	6:25	6:30	6:35	6:40

Updated 08.17.2023

**ROUTE 1 INBOUND**

# Lawrence-Haverhill via The Loop/Pleasant Valley St.

## WEEKDAYS

8	9	10	11	12	13	14	15	
Bus Starts at Washington Sq. Transit Station	Bus Leaves from Lowell & River	Bus Leaves from Pleasant Valley & Merrimack	Bus Leaves from The Loop	Bus Leaves from Methuen Plaza Walmart	Bus Leaves from Target Plaza	Bus Leaves from Jackson & Swan	Bus ends at Buckley Transportation Center	Bus continues on as Route
5:00	5:05	5:10	5:20	5:23	5:25	5:35	5:45	24
5:30	5:35	5:40	5:50	5:53	5:55	6:05	6:15	24
6:00	6:05	6:10	6:20	6:23	6:25	6:35	6:45	24
6:30	6:35	6:40	6:50	6:53	6:55	7:05	7:15	24
7:00	7:05	7:10	7:20	7:23	7:25	7:35	7:45	24
7:30	7:35	7:40	7:50	7:53	7:55	8:05	8:15	24
8:00	8:05	8:10	8:20	8:23	8:25	8:35	8:45	24
8:30	8:35	8:40	8:50	8:53	8:55	9:05	9:15	24
9:00	9:05	9:10	9:20	9:23	9:25	9:35	9:45	24
9:30	9:35	9:40	9:50	9:53	9:55	10:05	10:15	24
10:00	10:05	10:10	10:20	10:23	10:25	10:35	10:45	24
10:30	10:35	10:40	10:50	10:53	10:55	11:05	11:15	24
11:00	11:05	11:10	11:20	11:23	11:25	11:35	11:45	24
11:30	11:35	11:40	11:50	11:53	11:55	12:05	12:15	24
12:00	12:05	12:10	12:20	12:23	12:25	12:35	12:45	24
12:30	12:35	12:40	12:50	12:53	12:55	1:05	1:15	24
1:00	1:05	1:10	1:20	1:23	1:25	1:35	1:45	24
1:30	1:35	1:40	1:50	1:53	1:55	2:05	2:15	24
2:00	2:05	2:10	2:20	2:23	2:25	2:35	2:45	24
2:30	2:35	2:40	2:50	2:53	2:55	3:05	3:15	24
3:00	3:05	3:10	3:20	3:23	3:25	3:35	3:45	24
3:30	3:35	3:40	3:50	3:53	3:55	4:05	4:15	24
4:00	4:05	4:10	4:20	4:23	4:25	4:35	4:45	24
4:30	4:35	4:40	4:50	4:53	4:55	5:05	5:15	24
5:00	5:05	5:10	5:20	5:23	5:25	5:35	5:45	24
5:30	5:35	5:40	5:50	5:53	5:55	6:05	6:15	24
6:00	6:05	6:10	6:20	6:23	6:25	6:35	6:45	24
6:30	6:35	6:40	6:50	6:53	6:55	7:05	7:15	24
7:00	7:05	7:10	7:20	7:23	7:25	7:35	7:45	24
8:00	8:05	8:10	8:20	8:23	8:25	8:35	8:45	-
9:00	9:05	9:10	9:20	9:23	9:25	9:35	9:45	-

## SATURDAYS

7:00	7:05	7:10	7:20	7:23	7:25	7:35	7:45	24
8:00	8:05	8:10	8:20	8:23	8:25	8:35	8:45	24
9:00	9:05	9:10	9:20	9:23	9:25	9:35	9:45	24
10:00	10:05	10:10	10:20	10:23	10:25	10:35	10:45	24
10:30	10:35	10:40	10:50	10:53	10:55	11:05	11:15	24
11:00	11:05	11:10	11:20	11:23	11:25	11:35	11:45	24
11:30	11:35	11:40	11:50	11:53	11:55	12:05	12:15	24
12:00	12:05	12:10	12:20	12:23	12:25	12:35	12:45	24
12:30	12:35	12:40	12:50	12:53	12:55	1:05	1:15	24
1:00	1:05	1:10	1:20	1:23	1:25	1:35	1:45	24
1:30	1:35	1:40	1:50	1:53	1:55	2:05	2:15	24
2:00	2:05	2:10	2:20	2:23	2:25	2:35	2:45	24
2:30	2:35	2:40	2:50	2:53	2:55	3:05	3:15	24
3:00	3:05	3:10	3:20	3:23	3:25	3:35	3:45	24
3:30	3:35	3:40	3:50	3:53	3:55	4:05	4:15	24
4:00	4:05	4:10	4:20	4:23	4:25	4:35	4:45	24
4:30	4:35	4:40	4:50	4:53	4:55	5:05	5:15	24
5:00	5:05	5:10	5:20	5:23	5:25	5:35	5:45	24
6:00	6:05	6:10	6:20	6:23	6:25	6:35	6:45	-

Updated 08.17.2023



Merrimack Valley Regional Transit Authority  
85 Railroad Avenue | Haverhill, MA 01835

## Fixed Bus Route Information

### The Communities We Serve

The MVRTA fixed route bus system operates in the Merrimack Valley communities of Amesbury, Andover, Haverhill, Lawrence, Merrimac, Methuen, Newburyport, North Andover and Salisbury.

The MVRTA also provides service to the Lowell Transit Center for connections with the Lowell Regional Transit Authority.

### Fare Information

FREE

### Accessibility

The MVRTA's policy for governing the ADA DOT requirement to transport any wheelchair that does not exceed the capacities of the vehicle and its equipment (lift/ramp) is: Drivers must transport all passengers in wheelchairs whose combined weight and dimensions do not exceed the capacities of the vehicle and its equipment. Please note that if the combination of the customer and wheelchair/scooter exceeds the lift capacity, we may not be able to accommodate your trip.

- \* Service animals are permitted on all MVRTA vehicles.
- \* All schedules, brochures and applications are available in braille, audio and large print.

### Reasonable Modifications

The MVRTA is dedicated to providing equal access to its services for persons with disabilities as well as any individual who (either on occasions or over an extended period) may require modifications to the MVRTA's policy, practices and procedures. Any individual with disability requesting reasonable modification accommodations for extended period of time is required to complete the form listed on the MVRTA website or by calling (978) 469-6878 to request a form. A decision will be made within three (3) business days from the date of the request.

\* In the event that is not practical to make the request in advance, it can also be made with the reservationist (when reserving your trip) or directly with the driver (on the same). The reservationist, driver and dispatcher will then make a determination of whether the modification can be accommodated.

Violation of these policies could result in loss of riding privileges. In addition, several rules must be observed:

- All passengers are required to wear seatbelts. All wheelchairs and passengers are to be properly secured at all times. Passengers that are not properly secured will not be transported.
- Unsafe behavior or destruction of service property will be cause for immediate expulsion from the vehicle.
- Eating, drinking, smoking, or playing of loud music is not allowed.
- Tipping of drivers is not permitted.

### Fixed Bus Route & Schedule Information:

(978) 469-6878

[WWW.MVRTA.COM](http://WWW.MVRTA.COM)

We hope you will enjoy this service. If you have any questions, suggestions or concerns, contact:

Office of Special Services  
85 Railroad Avenue  
Haverhill, MA 01835

(978) 469-MVRTA (6878)  
option 3

[specialservices@MVRTA.com](mailto:specialservices@MVRTA.com)

Schedule & Route Information:  
(978) 469-MVRTA (6878)  
[www.MVRTA.com](http://www.MVRTA.com)

### What is The MVRTA?

The Merrimack Valley Regional Transit Authority (MVRTA) is a public transportation agency established under the Massachusetts General Law chapter 161B. Member cities and towns of the MVRTA are: Amesbury, Andover, Boxford, Georgetown, Groveland, Haverhill, Lawrence, Merrimac, Methuen, Newbury, Newburyport, North Andover, Rowley, Salisbury, and West Newbury. The MVRTA provides fixed route bus services, seniors and disabled transportation service, and commuter bus service.

The Merrimack Valley  
Regional Transit  
Authority Announces

## **Ring & Ride**

### What is Ring & Ride?

Ring & Ride is a curb-to-curb transportation service for the residents of Boxford, Georgetown, Groveland, Newbury, Byfield and West Newbury.

### Who Provides Ring & Ride?

The Merrimack Valley Regional Transit Authority provides this service through its operating company using wheelchair lift-equipped MVRTA vehicles.

Effective April 19, 2019

## What Trips Can I Take on Ring & Ride?

You can use the service in a variety of ways. Whether you are commuting to and from work, going shopping, visiting friends, or going to a medical appointment, Ring & Ride is there for you.

## Where Can I Go With Ring & Ride?

This service allows residents of Boxford, Georgetown, Groveland, Newbury/Byfield and West Newbury to commute anywhere in Amesbury, Boxford, Georgetown, Groveland, Haverhill, Lawrence, Methuen, Newbury/Byfield, Newburyport, North Andover and West Newbury, as well as to the Rowley Train Station and Market Basket in Rowley. This service will allow you to connect to the MVRTA fixed route bus system.

## When Does Ring & Ride operate?

### Ring & Ride Service Hours:

Monday – Friday 5:00 AM – 7:00 PM  
Saturday 9:00 AM – 6:00 PM

\* Service on Sunday is provided to Groveland Residents only. Sunday service hours are 9:00 AM – 6:00 PM.

Service is not available on the following holidays: New Year's Day, Martin Luther King Day, President's Day, Patriots Day, Memorial Day, Independence Day, Labor Day, Columbus Day, Veteran's Day, Thanksgiving Day, and Christmas Day.

## When and How Do I Reserve a Seat?

For reservations, please call 978-469-6878 option 3 Between 8:00 am and 4:30 pm Monday through Friday at least one day prior to service. Trips may be reserved up to two weeks in advance.

When you call, be prepared to provide the following information:

- Your name
- Your home, work, and/or cell phone number
- Your exact street address and requested appointment time.
- Your exact drop off location and, if you need a return trip, the return information.

Ring & Ride is a shared ride service intended to safely and effectively accommodate as many customers per trip as possible. You will be given a 30 minute pick-up window at the time you book your ride. Please be ready by the start of the pick-up window, and call the office of Special Services if your ride does not arrive by the end of the window. Severe weather or traffic conditions may result in the vehicle arriving later than expected. Upon arriving at your stop, the driver is permitted to wait no longer than five minutes for you to board the vehicle.

## How Do I Cancel My Ride?

You must call at least one hour before the start of your thirty minute pick-up window, weekdays between 7:00 am and 5:00 pm. Please call 978-469-6878 option 3. You may also cancel your trip after hours weekdays, or Saturday or Sunday by leaving a message on the voicemail at 978-469-6878 option 3.

## What Else Do I Need To Know About The Service?

There are no special identification cards needed to use Ring & Ride. Although rules may seem unnecessary for responsible adults, it is possible that a Ring & Ride customer may occasionally fail to observe several rules of etiquette. Therefore, in order to make this share ride service convenient for all customers, the policy for No-Shows and Late Cancellation is as follow:

**No-Show:** This disruption occurs when the MVRTA vehicle arrives at the specified location within a thirty minute window and the passenger is not ready or does not take the scheduled trip.

**Late Cancellations:** This disruption occurs when a passenger fails to notify MVRTA office of Special Services of a cancellation at least sixty minute prior to the start of your pick-up window.

**Disruption Penalties:** The MVRTA Office of Special Services has established the administrative process outlined below to suspend, for a reasonable period of time, the provision of complementary para-transit service to ADA eligible individuals who establish a pattern or practice of missing scheduled trips. Each individual trip history will be assessed to see if a pattern or practice of missing schedule trips exists.

Excessive No Show/Late Cancellations are considered excessive when a customer reserves 7 or more trips within any month and no-shows and/or late cancels 20 percent or more of those scheduled trips. At no time can a customer's no-show/late cancellations exceed 7 within one month without causing violation. This will be considered a pattern or practice of missing trips and the customer will be sent written notification that he/she has violated the

**Disruption Penalties Continued:**  
No-Show/Late Cancellation Policy and is subject to suspension.

\*The MVRTA Office of Special Services retains the discretion to impose service suspensions with any disruption that is considered inappropriate up to and including indefinite suspension for a first time disruption.

## What Does Ring & Ride Cost?

Ring & Ride Fare Rates Per one Way Trip Are As Follows:

	West Newbury	Newbury/Byfield	Groveland	Georgetown	Boxford	Amesbury
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Boxford
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Georgetown
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Groveland
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Haverhill
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Lawrence
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Methuen
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Newbury/Byfield
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Newburyport
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	North Andover
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	West Newbury
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Rowley Train Station
\$2.00	\$2.00	\$0.00	\$0.00	\$0.00	\$0.00	Rowley Market Basket

**VEHICLE TRAVEL SPEED DATA**

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: EB

Site Code: 98290001

9/21/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	MPH	
12:00 AM	0	0	0	4	14	8	4	1	0	0	0	0	0	31
1:00	0	0	0	3	7	3	0	0	0	0	0	0	0	13
2:00	0	0	0	3	2	1	2	0	0	0	0	0	0	8
3:00	0	0	0	2	4	2	2	1	0	0	0	0	0	11
4:00	0	0	2	7	11	6	1	1	0	0	0	0	0	28
5:00	0	0	0	11	23	18	5	2	0	0	0	0	0	59
6:00	0	0	3	24	63	44	20	3	0	0	0	0	0	157
7:00	0	0	6	37	126	87	18	4	0	0	0	0	0	278
8:00	1	0	16	88	138	89	22	0	1	0	0	0	0	355
9:00	0	2	18	80	151	72	10	0	0	0	0	0	0	333
10:00	0	3	34	104	156	78	7	0	0	0	0	0	0	382
11:00	0	0	36	119	153	49	9	1	0	0	0	0	0	367
12:00 PM	0	1	27	143	158	67	9	1	0	0	0	0	0	406
1:00	0	1	13	102	220	91	11	0	0	0	0	0	0	438
2:00	0	2	22	113	235	113	13	2	0	0	0	0	0	500
3:00	1	4	72	205	209	83	8	1	0	0	0	0	0	583
4:00	0	0	48	205	252	73	6	0	0	0	0	0	0	584
5:00	0	1	33	202	280	110	8	2	0	0	0	0	0	636
6:00	1	0	4	70	256	175	16	0	0	0	0	0	0	522
7:00	0	0	5	64	187	114	9	2	0	0	0	0	0	381
8:00	0	0	2	45	135	89	10	1	0	0	0	0	0	282
9:00	0	0	1	40	106	53	18	2	0	0	0	0	0	220
10:00	0	0	2	12	62	41	9	1	0	0	0	0	0	127
11:00	0	0	2	5	33	20	4	1	1	0	0	0	0	66
Total	3	14	346	1688	2981	1486	221	26	2	0	0	0	0	6767
	Percentile	15th	50th	85th	95th									
	Speed	28	33	37	40									
Mean Speed (Average)		32.2												
10 MPH Pace Speed		26-35												
Number in Pace		4633												
Percent in Pace		68.5%												
Number > 35 MPH		1735												
Percent > 35 MPH		25.6%												

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: EB

Site Code: 98290001

9/22/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	MPH	
12:00 AM	0	0	0	11	15	7	6	1	0	0	0	0	0	40
1:00	0	0	2	5	8	8	0	0	0	0	0	0	0	23
2:00	0	0	0	4	2	4	2	0	0	0	0	0	0	12
3:00	0	0	0	1	4	10	0	0	0	0	0	0	0	15
4:00	0	0	0	1	12	12	5	0	1	0	0	0	0	31
5:00	0	0	0	6	28	21	12	4	1	0	0	0	0	139
6:00	0	0	1	16	68	47	6	1	0	0	0	0	0	283
7:00	1	0	21	60	109	77	13	2	0	0	0	0	0	392
8:00	0	3	27	107	161	80	14	0	0	0	0	0	0	372
9:00	0	0	20	120	159	63	9	1	0	0	0	0	0	349
10:00	1	1	32	116	127	68	4	0	0	0	0	0	0	419
11:00	0	5	24	152	152	69	17	0	0	0	0	0	0	485
12:00 PM	0	1	42	178	177	72	15	0	0	0	0	0	0	453
1:00	3	1	21	163	180	76	7	2	0	0	0	0	0	620
2:00	0	1	41	211	286	70	11	0	0	0	0	0	0	741
3:00	0	3	56	271	307	94	8	2	0	0	0	0	0	685
4:00	0	1	76	266	250	78	13	1	0	0	0	0	0	561
5:00	0	0	24	177	258	92	9	0	1	0	0	0	0	529
6:00	2	0	15	150	238	112	11	1	0	0	0	0	0	416
7:00	0	0	10	158	176	62	9	1	0	0	0	0	0	280
8:00	0	0	10	76	126	61	6	0	0	1	0	0	0	195
9:00	0	0	3	34	94	48	13	3	0	0	0	0	0	158
10:00	0	0	2	29	70	48	5	4	0	0	0	0	0	27
11:00	0	0	0	7	9	7	4	0	0	0	0	0	0	7297
Total	7	16	427	2319	3016	1286	199	23	3	1	0	0	0	
	Percentile		15th	50th	85th	95th								
	Speed		27	32	36	39								
	Mean Speed (Average)		31.5											
	10 MPH Pace Speed		25-34											
	Number in Pace		5283											
	Percent in Pace		72.4%											
	Number > 35 MPH		1512											
	Percent > 35 MPH		20.7%											
Grand Total	10	30	773	4007	5997	2772	420	49	5	1	0	0	0	14064
	Percentile		15th	50th	85th	95th								
	Speed		28	32	37	40								
	Mean Speed (Average)		31.9											
	10 MPH Pace Speed		25-34											
	Number in Pace		9900											
	Percent in Pace		70.4%											
	Number > 35 MPH		3247											
	Percent > 35 MPH		23.1%											

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: WB

Site Code: 98290001

9/21/2023	0 - 15 MPH	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
12:00 AM	0	0	0	1	6	5	5	3	2	0	0	0	0	22
1:00	0	0	0	1	4	8	4	1	0	0	0	0	0	18
2:00	0	0	0	0	2	3	2	1	0	0	0	0	0	8
3:00	0	0	0	6	5	4	3	0	0	0	0	0	0	18
4:00	0	0	0	5	13	22	10	2	0	0	0	0	0	52
5:00	1	0	10	13	48	37	19	2	5	0	0	0	0	310
6:00	0	1	7	35	82	120	55	8	2	0	0	0	0	473
7:00	1	1	13	40	121	201	77	18	1	0	0	0	0	442
8:00	8	5	13	38	136	161	73	7	1	0	0	0	0	368
9:00	1	5	7	32	114	149	52	8	0	0	0	0	0	384
10:00	0	0	4	40	138	161	35	5	0	1	0	0	0	484
11:00	0	1	9	49	199	165	51	10	0	0	0	0	0	437
12:00 PM	1	0	6	38	139	172	71	9	1	0	0	0	0	466
1:00	3	0	6	33	125	207	86	5	1	0	0	0	0	434
2:00	0	0	5	35	136	189	57	10	2	0	0	0	0	492
3:00	6	8	15	35	163	182	77	6	0	0	0	0	0	585
4:00	0	0	6	32	153	275	97	18	3	1	0	0	0	558
5:00	2	1	5	49	214	198	84	5	0	0	0	0	0	447
6:00	0	1	6	35	164	191	38	11	1	0	0	0	0	271
7:00	1	0	4	25	106	107	21	7	0	0	0	0	0	235
8:00	0	0	4	21	87	86	30	5	2	0	0	0	0	129
9:00	3	0	1	13	41	53	17	1	0	0	0	0	0	85
10:00	0	0	3	8	19	37	15	2	1	0	0	0	0	38
11:00	0	0	1	7	11	9	8	1	1	0	0	0	0	6891
Total	27	23	125	591	2226	2742	987	145	23	2	0	0	0	
	Percentile	15th	50th	85th	95th									
	Speed	32	36	41	44									
Mean Speed (Average)		35.6												
10 MPH Pace Speed		30-39												
Number in Pace		4925												
Percent in Pace		71.5%												
Number > 35 MPH		3899												
Percent > 35 MPH		56.6%												

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: WB

Site Code: 98290001

9/22/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	MPH	
12:00 AM	0	0	0	2	8	5	4	1	0	0	0	0	0	20
1:00	0	0	1	0	2	3	3	4	0	0	0	0	0	13
2:00	0	0	0	1	10	1	0	1	0	0	0	0	0	13
3:00	0	0	2	0	8	7	1	3	0	0	0	0	0	21
4:00	0	0	2	2	19	19	9	5	2	1	0	0	0	59
5:00	0	0	9	16	33	44	19	6	1	0	0	0	0	284
6:00	0	0	7	25	79	116	48	9	0	0	0	0	0	431
7:00	0	2	13	28	101	178	93	12	3	1	0	0	0	440
8:00	0	0	16	48	108	171	81	12	4	0	0	0	0	384
9:00	0	1	12	31	113	151	62	10	4	0	0	0	0	394
10:00	0	0	7	51	100	169	57	9	1	0	0	0	0	429
11:00	0	1	10	34	132	175	67	9	1	0	0	0	0	463
12:00 PM	0	2	3	20	142	225	59	8	4	0	0	0	0	449
1:00	0	3	8	25	132	202	71	7	1	0	0	0	0	540
2:00	1	2	22	49	171	213	75	7	0	0	0	0	0	509
3:00	0	4	13	58	150	205	68	9	2	0	0	0	0	595
4:00	3	6	23	60	162	237	90	10	4	0	0	0	0	555
5:00	1	1	11	55	188	217	71	11	0	0	0	0	0	459
6:00	0	1	8	63	141	185	51	8	2	0	0	0	0	286
7:00	1	3	7	51	126	70	22	5	1	0	0	0	0	213
8:00	0	2	6	25	71	75	27	6	1	0	0	0	0	158
9:00	1	0	4	11	54	68	18	1	1	0	0	0	0	111
10:00	0	0	1	10	29	43	24	2	1	1	0	0	0	19
11:00	0	0	0	0	8	7	3	1	0	0	0	0	0	6973
Total	7	28	185	665	2087	2786	1023	156	33	3	0	0	0	
	Percentile Speed	15th	50th	85th	95th									
	Mean Speed (Average)	35.6												
	10 MPH Pace Speed	30-39												
	Number in Pace	4831												
	Percent in Pace	69.3%												
	Number > 35 MPH	4001												
	Percent > 35 MPH	57.4%												
Grand Total	34	51	310	1256	4313	5528	2010	301	56	5	0	0	0	13864
	Percentile Speed	15th	50th	85th	95th									
	Mean Speed (Average)	35.6												
	10 MPH Pace Speed	30-39												
	Number in Pace	9756												
	Percent in Pace	70.4%												
	Number > 35 MPH	7900												
	Percent > 35 MPH	57.0%												

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: Combined

Site Code: 98290001

9/21/2023	0 - 15 MPH	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
12:00 AM	0	0	0	5	20	13	9	4	2	0	0	0	0	53
1:00	0	0	0	4	11	11	4	1	0	0	0	0	0	31
2:00	0	0	0	3	4	4	4	1	0	0	0	0	0	16
3:00	0	0	0	8	9	6	5	1	0	0	0	0	0	29
4:00	0	0	2	12	24	28	11	3	0	0	0	0	0	80
5:00	1	0	10	24	71	55	24	4	5	0	0	0	0	194
6:00	0	1	10	59	145	164	75	11	2	0	0	0	0	467
7:00	1	1	19	77	247	288	95	22	1	0	0	0	0	751
8:00	9	5	29	126	274	250	95	7	2	0	0	0	0	797
9:00	1	7	25	112	265	221	62	8	0	0	0	0	0	701
10:00	0	3	38	144	294	239	42	5	0	1	0	0	0	766
11:00	0	1	45	168	352	214	60	11	0	0	0	0	0	851
12:00 PM	1	1	33	181	297	239	80	10	1	0	0	0	0	843
1:00	3	1	19	135	345	298	97	5	1	0	0	0	0	904
2:00	0	2	27	148	371	302	70	12	2	0	0	0	0	934
3:00	7	12	87	240	372	265	85	7	0	0	0	0	0	1075
4:00	0	0	54	237	405	348	103	18	3	1	0	0	0	1169
5:00	2	2	38	251	494	308	92	7	0	0	0	0	0	1194
6:00	1	1	10	105	420	366	54	11	1	0	0	0	0	969
7:00	1	0	9	89	293	221	30	9	0	0	0	0	0	652
8:00	0	0	6	66	222	175	40	6	2	0	0	0	0	517
9:00	3	0	2	53	147	106	35	3	0	0	0	0	0	349
10:00	0	0	5	20	81	78	24	3	1	0	0	0	0	212
11:00	0	0	3	12	44	29	12	2	2	0	0	0	0	104
Total	30	37	471	2279	5207	4228	1208	171	25	2	0	0	0	13658
	Percentile Speed	15th	50th	85th	95th									
	Mean Speed (Average)	33.9												
	10 MPH Pace Speed	30-39												
	Number in Pace	9396												
	Percent in Pace	68.8%												
	Number > 35 MPH	5634												
	Percent > 35 MPH	41.3%												

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: Combined

Site Code: 98290001

9/22/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 - 75 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	75 MPH	
12:00 AM	0	0	0	13	23	12	10	2	0	0	0	0	0	60
1:00	0	0	3	5	10	11	3	4	0	0	0	0	0	36
2:00	0	0	0	5	12	5	2	1	0	0	0	0	0	25
3:00	0	0	2	1	12	17	1	3	0	0	0	0	0	36
4:00	0	0	2	3	31	31	14	5	3	1	0	0	0	90
5:00	0	0	9	22	61	65	31	10	2	0	0	0	0	423
6:00	0	0	8	41	147	163	54	10	0	0	0	0	0	714
7:00	1	2	34	88	210	255	106	14	3	1	0	0	0	832
8:00	0	3	43	155	269	251	95	12	4	0	0	0	0	756
9:00	0	1	32	151	272	214	71	11	4	0	0	0	0	743
10:00	1	1	39	167	227	237	61	9	1	0	0	0	0	848
11:00	0	6	34	186	284	244	84	9	1	0	0	0	0	948
12:00 PM	0	3	45	198	319	297	74	8	4	0	0	0	0	902
1:00	3	4	29	188	312	278	78	9	1	0	0	0	0	1160
2:00	1	3	63	260	457	283	86	7	0	0	0	0	0	1250
3:00	0	7	69	329	457	299	76	11	2	0	0	0	0	1280
4:00	3	7	99	326	412	315	103	11	4	0	0	0	0	1116
5:00	1	1	35	232	446	309	80	11	1	0	0	0	0	988
6:00	2	1	23	213	379	297	62	9	2	0	0	0	0	702
7:00	1	3	17	209	302	132	31	6	1	0	0	0	0	493
8:00	0	2	16	101	197	136	33	6	1	1	0	0	0	353
9:00	1	0	7	45	148	116	31	4	1	0	0	0	0	269
10:00	0	0	3	39	99	91	29	6	1	1	0	0	0	46
11:00	0	0	0	7	17	14	7	1	0	0	0	0	0	
Total	14	44	612	2984	5103	4072	1222	179	36	4	0	0	0	14270
		Percentile Speed	15th	50th	85th	95th								
		Mean Speed (Average)	29	34	39	42								
		10 MPH Pace Speed	33.5											
		Number in Pace	30-39											
		Percent in Pace	9153											
		Number > 35 MPH	64.1%											
		Percent > 35 MPH	5513											
			38.6%											
Grand Total	44	81	1083	5263	10310	8300	2430	350	61	6	0	0	0	27928
		Percentile Speed	15th	50th	85th	95th								
		Mean Speed (Average)	29	34	39	42								
		10 MPH Pace Speed	33.7											
		Number in Pace	30-39											
		Percent in Pace	18549											
		Number > 35 MPH	66.4%											
		Percent > 35 MPH	11147											
			39.9%											

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: EB

Site Code: 982900S1

9/30/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	MPH	
12:00 AM	0	0	2	12	20	11	2	0	0	0	0	0	0	47
1:00	0	0	3	8	11	5	2	1	0	0	0	0	0	30
2:00	0	0	0	2	8	8	0	1	0	0	0	0	0	14
3:00	0	0	0	3	6	2	3	0	0	0	0	0	0	15
4:00	0	0	0	5	5	4	1	0	0	0	0	0	0	26
5:00	0	0	3	8	10	2	2	1	0	0	0	0	0	53
6:00	0	0	0	10	21	16	6	0	0	0	0	0	0	138
7:00	0	0	0	14	77	37	7	2	1	0	0	0	0	220
8:00	0	1	0	35	96	62	21	5	0	0	0	0	0	331
9:00	0	0	0	30	175	108	15	3	0	0	0	0	0	472
10:00	0	1	10	48	249	141	20	3	0	0	0	0	0	459
11:00	0	0	0	80	244	126	7	1	0	0	0	1	0	579
12:00 PM	0	0	7	92	315	137	27	0	0	0	0	1	0	556
1:00	0	0	13	55	312	142	33	1	0	0	0	0	0	514
2:00	1	0	6	69	285	130	18	5	0	0	0	0	0	506
3:00	0	0	4	51	279	144	24	4	0	0	0	0	0	472
4:00	2	0	14	70	223	146	15	1	1	0	0	0	0	417
5:00	1	4	11	71	244	121	20	0	0	0	0	0	0	284
6:00	0	1	4	82	212	97	19	2	0	0	0	0	0	284
7:00	0	1	11	55	136	70	9	2	0	0	0	0	0	218
8:00	2	0	3	46	156	66	10	0	1	0	0	0	0	136
9:00	3	1	2	35	111	58	6	2	0	0	0	0	0	34
10:00	2	0	8	34	63	24	4	1	0	0	0	0	0	6296
11:00	0	0	0	8	18	6	2	0	0	0	0	0	0	6296
Total	11	9	101	923	3276	1663	273	35	3	0	0	2	0	
Grand Total	11	9	101	923	3276	1663	273	35	3	0	0	2	0	

Stats	Percentile Speed	15th	50th	85th	95th
	Mean Speed (Average)	33.4			
	10 MPH Pace Speed	30-39			
	Number in Pace	4924			
	Percent in Pace	78.2%			
	Number > 35 MPH	1976			
	Percent > 35 MPH	31.4%			

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: WB

Site Code: 982900S1

9/30/2023	0 - 15	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
Time	MPH	20 MPH	25 MPH	30 MPH	35 MPH	40 MPH	45 MPH	50 MPH	55 MPH	60 MPH	65 MPH	70 MPH	0	46
12:00 AM	1	0	2	5	15	17	5	1	0	0	0	0	0	0
1:00	0	0	0	4	14	6	3	2	0	0	0	0	0	29
2:00	0	0	0	3	4	5	3	0	0	0	0	0	0	15
3:00	0	0	0	0	2	7	4	0	0	0	0	0	0	13
4:00	0	0	1	2	8	12	2	0	0	0	0	0	0	34
5:00	0	1	0	2	16	11	3	0	1	0	0	0	2	95
6:00	0	0	0	3	39	39	10	2	0	0	0	1	0	179
7:00	0	0	0	5	61	79	29	4	0	0	0	0	0	297
8:00	0	0	6	19	68	153	41	8	0	0	0	0	0	422
9:00	0	0	1	35	132	186	61	3	4	0	0	0	0	511
10:00	1	1	2	25	194	236	47	4	1	0	0	0	0	572
11:00	0	0	2	31	195	295	47	2	0	0	0	0	0	600
12:00 PM	0	0	2	22	227	280	62	6	0	0	1	0	0	492
1:00	0	1	7	25	169	222	62	4	0	2	0	0	0	467
2:00	1	0	1	23	157	226	55	4	0	0	0	0	0	433
3:00	0	0	2	19	171	191	43	7	0	0	0	0	0	456
4:00	1	0	9	30	161	202	49	3	0	1	0	0	0	412
5:00	4	2	1	21	140	197	40	7	0	0	0	0	0	375
6:00	0	3	1	24	174	148	25	0	0	0	0	0	0	248
7:00	1	0	1	35	118	69	22	2	0	0	0	0	0	202
8:00	3	0	0	12	86	75	23	3	0	0	0	0	0	129
9:00	5	0	1	12	38	55	14	3	0	0	0	0	0	103
10:00	3	2	1	18	40	32	6	1	0	0	0	0	0	25
11:00	0	0	0	2	9	8	3	2	0	1	0	0	0	6181
Total	20	10	40	377	2238	2751	659	68	6	4	2	0	6	6181
Grand Total	20	10	40	377	2238	2751	659	68	6	4	2	0	6	6181
Stats	Percentile	15th	50th	85th	95th									
	Speed	32	35	40	42									
Mean Speed (Average)		35.7												
10 MPH Pace Speed		30-39												
Number in Pace		4942												
Percent in Pace		80.0%												
Number > 35 MPH		3496												
Percent > 35 MPH		56.6%												

Accurate Counts  
978-664-2565

Location : Pleasant Valley Street  
Location : West of Route 213  
City/State: Methuen, MA  
Direction: Combined

Site Code: 982900S1

9/30/2023	0 - 15 MPH	> 15 - 20 MPH	> 20 - 25 MPH	> 25 - 30 MPH	> 30 - 35 MPH	> 35 - 40 MPH	> 40 - 45 MPH	> 45 - 50 MPH	> 50 - 55 MPH	> 55 - 60 MPH	> 60 - 65 MPH	> 65 - 70 MPH	> 70 MPH	Total
12:00 AM	1	0	4	17	35	28	7	1	0	0	0	0	0	93
1:00	0	0	3	12	25	11	5	3	0	0	0	0	0	59
2:00	0	0	0	5	12	13	3	1	0	0	0	0	0	34
3:00	0	0	0	3	8	9	7	0	0	0	0	0	0	27
4:00	0	0	1	7	13	16	3	0	0	0	0	0	1	41
5:00	0	1	3	10	26	13	5	1	1	0	0	0	0	60
6:00	0	0	0	13	60	55	16	2	0	0	0	0	2	148
7:00	0	0	0	19	138	116	36	6	1	0	1	0	0	317
8:00	0	1	6	54	164	215	62	13	0	0	0	0	2	517
9:00	0	0	1	65	307	294	76	6	4	0	0	0	0	753
10:00	1	2	12	73	443	377	67	7	1	0	0	0	0	983
11:00	0	0	2	111	439	421	54	3	0	0	0	1	0	1031
12:00 PM	0	0	9	114	542	417	89	6	0	0	1	1	0	1179
1:00	0	1	20	80	481	364	95	5	0	2	0	0	0	1048
2:00	2	0	7	92	442	356	73	9	0	0	0	0	0	981
3:00	0	0	6	70	450	335	67	11	0	0	0	0	0	939
4:00	3	0	23	100	384	348	64	4	1	1	0	0	0	928
5:00	5	6	12	92	384	318	60	7	0	0	0	0	0	884
6:00	0	4	5	106	386	245	44	2	0	0	0	0	0	792
7:00	1	1	12	90	254	139	31	4	0	0	0	0	0	532
8:00	5	0	3	58	242	141	33	3	1	0	0	0	0	486
9:00	8	1	3	47	149	113	20	5	0	0	0	0	1	347
10:00	5	2	9	52	103	56	10	2	0	0	0	0	0	239
11:00	0	0	0	10	27	14	5	2	0	1	0	0	0	59
Total	31	19	141	1300	5514	4414	932	103	9	4	2	2	6	12477
Grand Total	31	19	141	1300	5514	4414	932	103	9	4	2	2	6	12477
Stats	Percentile Speed	15th	50th	85th	95th									
	Mean Speed (Average)	34.6												
	10 MPH Pace Speed	30-39												
	Number in Pace	9866												
	Percent in Pace	79.1%												
	Number > 35 MPH	5472												
	Percent > 35 MPH	43.9%												

MASSDOT CRASH RATE WORKSHEET AND HIGH CRASH LOCATION MAPPING



## INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Methuen COUNT DATE : 9/21/2023

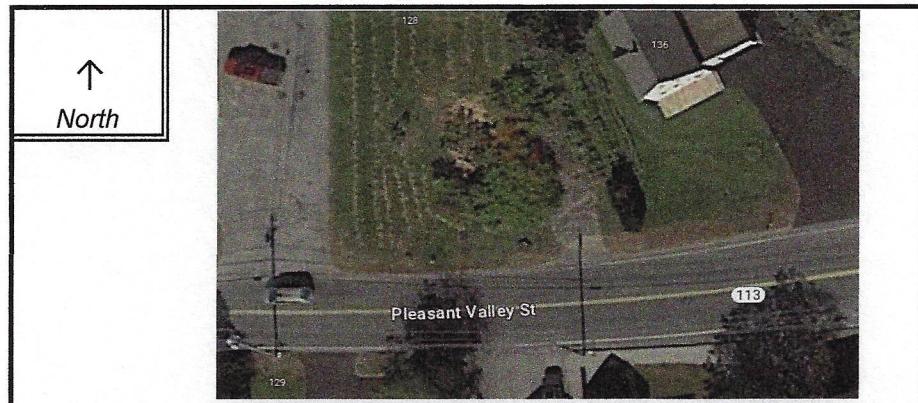
DISTRICT : 4 UNSIGNALIZED :  SIGNALIZED :

### ~ INTERSECTION DATA ~

MAJOR STREET : Pleasant Valley Street (Route 113)

MINOR STREET(S) : 128 Pleasant Valley Street Driveway

INTERSECTION  
DIAGRAM  
(Label Approaches)



### PEAK HOUR VOLUMES

APPROACH :	1	2	3	4	5	Total Peak Hourly Approach Volume
DIRECTION :	NB	SB	EB	WB		
PEAK HOURLY VOLUMES (PM) :	-	0	610	605		1,215

"K" FACTOR : 0.090 INTERSECTION ADT (V) = TOTAL DAILY APPROACH VOLUME : 13,500

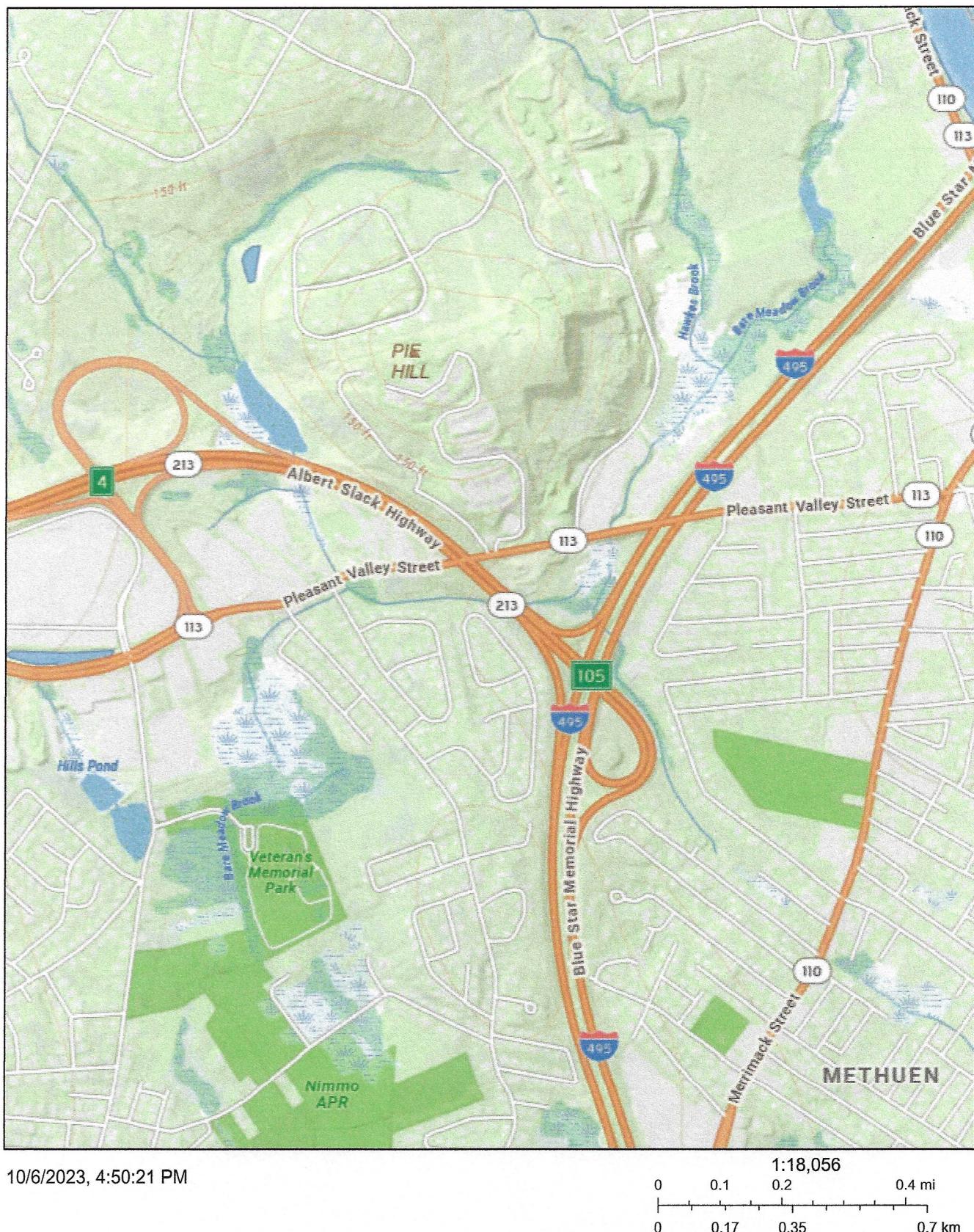
TOTAL # OF CRASHES : 1 # OF YEARS : 5 AVERAGE # OF CRASHES PER YEAR (A) : 0.20

CRASH RATE CALCULATION : 0.04 RATE = 
$$\frac{(A * 1,000,000)}{(V * 365)}$$

Comments : Below MassDOT Statewide and District Average Crash Rates

Project Title & Date: 9829 - Proposed Car Wash

# MassDOT Top Crash Locations



10/6/2023, 4:50:21 PM

## GENERAL BACKGROUND TRAFFIC GROWTH

Proposed Car Wash, Methuen, MA

**General Background Traffic Growth - Daily Traffic Volumes**

CITY/TOWN	ROUTE/STREET	LOCATION	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	Annual Growth	
Methuen	Pleasant Valley Street (Route 113)	West of I-495						11,944	12,219	12,977	13,198	13,238	13,185	2.02%	
Methuen	Albert Slack Highway	West of I-495	49,972	50,122	53,370	53,002	52,638	53,480	55,619	58,289	58,755	59,343	60,530	1.96%	
Methuen	Ramp - I-495 SB to Route 213 WB	Exit 47, Route 213					14,910	14,578	14,491	14,839		15,817	14,984	-1.42%	
Methuen	Ramp - I-495 NB to Route 213 WB	Exit 47, Route 214					12,523	11,418	11,601	12,065	12,644	12,745	12,872	-1.24%	
Methuen	Ramp - Route 213 EB to I-495 NB	Exit 5B, I-495					16,119	15,510	15,758	16,388	17,175	17,312	17,485	-1.54%	
Methuen	Ramp - Route 213 EB to I-495 SB	Exit 5A, I-496					11,192	11,125	11,392			12,143	11,445	-1.32%	
Methuen	I-495	Between Routes 113 and 213 Connector	105,714	107,841	109,935	109,430	108,773	109,907	120,167	119,410	121,436	118,397	118,397	1.32%	
Methuen	Milk Street	South of Pleasant Valley Street (Route 113)										5,449	5,427	-0.40%	
Methuen	Pleasant Valley Street (Route 113)	East of Prospect Street					14,543	14,994	15,339	16,310	16,587	16,637	16,570	2.22%	
Methuen	Ramp - Route 113 to Route 213 EB	Pleasant Valley Street (Route 113)					5,062	5,056	5,137	5,342			5,694	5,671	1.27%
Methuen	Ramp - Route 213 EB to Route 113	Exit 4, Route 113					4,869	4,867	4,945	5,143			5,482	5,460	1.29%
Methuen	Ramp - Route 113 to Route 213 WB	Pleasant Valley Street (Route 113)					3,762	3,761	3,878	3,967	4,213	4,285	4,298	4,281	1.89%
Methuen	Ramp - Route 213 WB to Route 113	Exit 4, Route 113					4,709	4,707	4,853	4,965	5,273	5,363	5,379	5,357	1.88%
Methuen	East Street	East of I-495	16,200	16,102	16,723	15,476	15,507	15,988	15,729	16,704	16,988	17,679	17,608	0.99%	
														0.63%	

## TRIP-GENERATION CALCUALTIONS



## Graph Look Up

ITETripGen Web-based App

Graph Look Up

How to Use ITETripGen

TGM Desk Reference

TGM Appendices

Support Documents

Add Users

Comments

Add-ons to do more

Try OTISS Pro

Query Filter

**DATA SOURCE:** Trip Generation Manual, 11th Ed

**SEARCH BY LAND USE CODE:** 948

**LAND USE GROUP:** (900-999) Services

**LAND USE:** 948 - Automated Car Wash

**LAND USE SUBCATEGORY:** All Sites

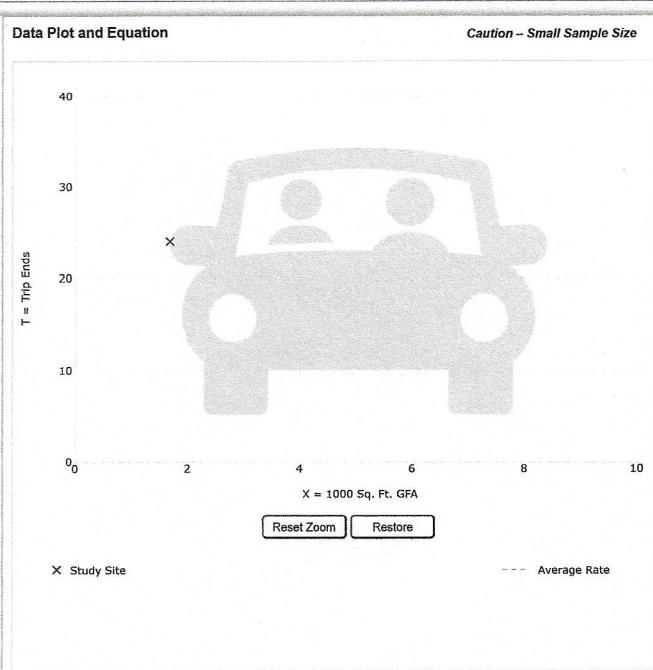
**SETTING/LOCATION:** General Urban/Suburban

**INDEPENDENT VARIABLE (IV):** 1000 Sq. Ft. GFA

**TIME PERIOD:** Weekday, Peak Hour of Adjacent Street Traffic

**TRIP TYPE:** Vehicle

**ENTER IV VALUE TO CALCULATE TRIPS:** 1.5



DATA STATISTICS	
<b>Land Use:</b>	Automated Car Wash (948) <a href="#">Click for Description and Data Plots</a>
<b>Independent Variable:</b>	1000 Sq. Ft. GFA
<b>Time Period:</b>	Weekday
<b>Peak Hour of Adjacent Street Traffic</b>	One Hour Between 4 and 6 p.m.
<b>Setting/Location:</b>	General Urban/Suburban
<b>Trip Type:</b>	Vehicle
<b>Number of Studies:</b>	1
<b>Avg. 1000 Sq. Ft. GFA:</b>	2
<b>Average Rate:</b>	14.20
<b>Range of Rates:</b>	14.20 - 14.20
<b>Standard Deviation:</b>	***
<b>Fitted Curve Equation:</b>	Not Given
<b>R<sup>2</sup>:</b>	***
<b>Directional Distribution:</b>	50% entering, 50% exiting
<b>Calculated Trip Ends:</b>	Average Rate: 21 (Total), 11 (Entry), 10 (Exit)



## Graph Look Up

ITETripGen Web-based App

Graph Look Up

How to Use ITETripGen

TGM Desk Reference

TGM Appendices

Support Documents

Add Users

Comments

Add-ons to do more

Try OTISS Pro

Query Filter

DATA SOURCE:

Trip Generation Manual, 11th Ed

SEARCH BY LAND USE CODE:

948



LAND USE GROUP:

(900-999) Services

LAND USE:

948 - Automated Car Wash

LAND USE SUBCATEGORY:

All Sites

SETTING/LOCATION:

General Urban/Suburban

INDEPENDENT VARIABLE (IV):

1000 Sq. Ft. GFA

TIME PERIOD:

Saturday, Peak Hour of Generator

TRIP TYPE:

Vehicle

ENTER IV VALUE TO CALCULATE TRIPS:

1.5

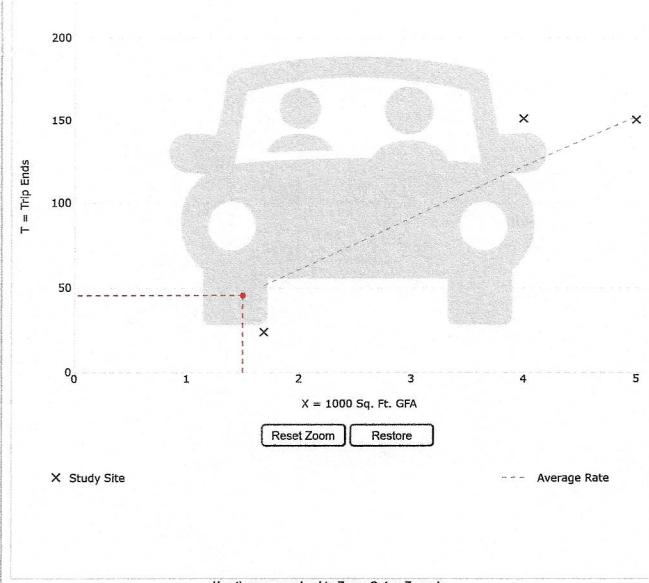
Calculate

## Data Plot and Equation

## Caution – Small Sample Size

## DATA STATISTICS

Land Use:  
Automated Car Wash (948) [Click for Description and Data Plots](#)

Independent Variable:  
1000 Sq. Ft. GFATime Period:  
Saturday  
Peak Hour of GeneratorSetting/Location:  
General Urban/SuburbanTrip Type:  
VehicleNumber of Studies:  
3Avg. 1000 Sq. Ft. GFA:  
4Average Rate:  
30.40Range of Rates:  
14.20 - 37.75Standard Deviation:  
9.63Fitted Curve Equation:  
Not GivenR<sup>2</sup>:  
\*\*\*\*Directional Distribution:  
50% entering, 50% exitingCalculated Trip Ends:  
Average Rate: 46 (Total), 23 (Entry), 23 (Exit)

## Proposed Car Wash

### Theoretical Daily Rate

ITE LUC 947 Average Weekday Rate = 108.00

ITE LUC 947 Weekday Evening Peak Hour Rate = 5.54

ITE LUC 948 Weekday Evening Peak Hour Rate = 14.20

ITE LUC 948 PM  $\times \frac{\text{ITE LUC 947 Avg. Weekday}}{\text{ITE LUC 947 PM}} = \text{Theoretical Avg. Weekday Rate}$

$$14.20 \times \frac{108.00}{5.54} = 276.82$$

$$T = 1.500 \times 276.82 = 415.23$$

$$T \approx 416 [208 \text{ Enter} - 208 \text{ Exit}]$$

### Weekday Morning Peak-Hour Traffic Volumes

ITE LUC 947 Average Weekday Rate = 108.00

ITE LUC 947 Weekday Morning Peak Hour Rate = 8.00 (50% Entering, 50% Exiting)

% of Daily Total During AM Peak Hour =  $\frac{8.00}{108.00} = 7.4\% \text{ of Daily Entering Traffic}$

$$\text{Calculated Daily Traffic} = 416 [208 \text{ Enter} - 208 \text{ Exit}]$$

$$416 \times 0.074 = 30.78 \approx 31$$

$$T = 31 [16 \text{ Entering} - 15 \text{ Exiting}]$$

**CAPACITY ANALYSIS WORKSHEETS**



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	0	314	501	0	0	0
Future Volume (vph)	0	314	501	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr						
Flt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Flt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	388	563	0	0	0
Lane Group Flow (vph)	0	388	563	0	0	0
Sign Control	Free	Free		Stop		
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	0	314	501	0	0	0
Future Vol, veh/h	0	314	501	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	81	81	89	89	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	388	563	0	0	0
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	563	0	-	0	951	563
Stage 1	-	-	-	-	563	-
Stage 2	-	-	-	-	388	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	1008	-	-	-	288	526
Stage 1	-	-	-	-	570	-
Stage 2	-	-	-	-	686	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	1008	-	-	-	288	526
Mov Cap-2 Maneuver	-	-	-	-	288	-
Stage 1	-	-	-	-	570	-
Stage 2	-	-	-	-	686	-
Approach	EB	WB	SB			
HCM Control Delay, s	0	0	0			
HCM LOS			A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	1008	-	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	-	-	0
HCM Lane LOS	A	-	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	-	-



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	0	610	605	0	0	0
Future Volume (vph)	0	610	605	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr						
Flt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Flt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	685	630	0	0	0
Lane Group Flow (vph)	0	685	630	0	0	0
Sign Control	Free	Free		Stop		
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↑	↑	↔		
Traffic Vol, veh/h	0	610	605	0	0	0
Future Vol, veh/h	0	610	605	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	89	89	96	96	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	685	630	0	0	0
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	630	0	-	0	1315	630
Stage 1	-	-	-	-	630	-
Stage 2	-	-	-	-	685	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	952	-	-	-	174	482
Stage 1	-	-	-	-	531	-
Stage 2	-	-	-	-	500	-
Platoon blocked, %	-	-	-	-		
Mov Cap-1 Maneuver	952	-	-	-	174	482
Mov Cap-2 Maneuver	-	-	-	-	174	-
Stage 1	-	-	-	-	531	-
Stage 2	-	-	-	-	500	-
Approach	EB	WB	SB			
HCM Control Delay, s	0	0	0			
HCM LOS			A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	952	-	-	-	-	
HCM Lane V/C Ratio	-	-	-	-	-	
HCM Control Delay (s)	0	-	-	-	0	
HCM Lane LOS	A	-	-	-	A	
HCM 95th %tile Q(veh)	0	-	-	-	-	

2023 Existing Saturday Midday  
3: Route 113 & Site Driveway

10/10/2023



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	0	600	580	0	0	0
Future Volume (vph)	0	600	580	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr1						
Flt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Flt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	659	611	0	0	0
Lane Group Flow (vph)	0	659	611	0	0	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↖ ↗	↖ ↗	↖ ↗		
Traffic Vol, veh/h	0	600	580	0	0	0
Future Vol, veh/h	0	600	580	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	91	91	95	95	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	659	611	0	0	0
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	611	0	-	0	1270	611
Stage 1	-	-	-	-	611	-
Stage 2	-	-	-	-	659	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	968	-	-	-	186	494
Stage 1	-	-	-	-	542	-
Stage 2	-	-	-	-	515	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	968	-	-	-	186	494
Mov Cap-2 Maneuver	-	-	-	-	186	-
Stage 1	-	-	-	-	542	-
Stage 2	-	-	-	-	515	-
Approach	EB	WB	SB			
HCM Control Delay, s	0	0	0			
HCM LOS			A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	968	-	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	-	-	0
HCM Lane LOS	A	-	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	-	-



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	0	337	537	0	0	0
Future Volume (vph)	0	337	537	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Frt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Frt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	416	603	0	0	0
Lane Group Flow (vph)	0	416	603	0	0	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Control Type: Unsignalized						

Intersection							
Int Delay, s/veh	0	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations							
Traffic Vol, veh/h	0	337	537	0	0	0	0
Future Vol, veh/h	0	337	537	0	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop	
RT Channelized	-	None	-	None	-	None	
Storage Length	-	-	-	-	0	-	
Veh in Median Storage, #	-	0	0	-	0	-	
Grade, %	-	0	0	-	0	-	
Peak Hour Factor	81	81	89	89	92	92	
Heavy Vehicles, %	2	2	2	2	2	2	
Mvmt Flow	0	416	603	0	0	0	
Major/Minor	Major1	Major2	Minor2				
Conflicting Flow All	603	0	-	0	1019	603	
Stage 1	-	-	-	-	603	-	
Stage 2	-	-	-	-	416	-	
Critical Hdwy	4.12	-	-	-	6.42	6.22	
Critical Hdwy Stg 1	-	-	-	-	5.42	-	
Critical Hdwy Stg 2	-	-	-	-	5.42	-	
Follow-up Hdwy	2.218	-	-	-	3.518	3.318	
Pot Cap-1 Maneuver	975	-	-	-	263	499	
Stage 1	-	-	-	-	546	-	
Stage 2	-	-	-	-	666	-	
Platoon blocked, %	-	-	-	-			
Mov Cap-1 Maneuver	975	-	-	-	263	499	
Mov Cap-2 Maneuver	-	-	-	-	263	-	
Stage 1	-	-	-	-	546	-	
Stage 2	-	-	-	-	666	-	
Approach	EB	WB	SB				
HCM Control Delay, s	0	0	-	0			
HCM LOS			-	A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1		
Capacity (veh/h)	975	-	-	-	-		
HCM Lane V/C Ratio	-	-	-	-	-		
HCM Control Delay (s)	0	-	-	-	0		
HCM Lane LOS	A	-	-	-	A		
HCM 95th %tile Q(veh)	0	-	-	-	-		



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↑	↑		↑	
Traffic Volume (vph)	0	654	649	0	0	0
Future Volume (vph)	0	654	649	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Flt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Flt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	735	676	0	0	0
Lane Group Flow (vph)	0	735	676	0	0	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		↖ ↗	↖ ↗	↖ ↗		
Traffic Vol, veh/h	0	654	649	0	0	0
Future Vol, veh/h	0	654	649	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	89	89	96	96	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	735	676	0	0	0
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	676	0	-	0	1411	676
Stage 1	-	-	-	-	676	-
Stage 2	-	-	-	-	735	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	915	-	-	-	152	453
Stage 1	-	-	-	-	505	-
Stage 2	-	-	-	-	474	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	915	-	-	-	152	453
Mov Cap-2 Maneuver	-	-	-	-	152	-
Stage 1	-	-	-	-	505	-
Stage 2	-	-	-	-	474	-
Approach	EB	WB	SB			
HCM Control Delay, s	0	0	0			
HCM LOS			A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	915	-	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	-	0	-
HCM Lane LOS	A	-	-	-	A	-
HCM 95th %tile Q(veh)	0	-	-	-	-	-



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	0	643	622	0	0	0
Future Volume (vph)	0	643	622	0	0	0
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr						
Flt Protected						
Satd. Flow (prot)	0	1987	2111	0	1614	0
Flt Permitted						
Satd. Flow (perm)	0	1987	2111	0	1614	0
Adj. Flow (vph)	0	707	655	0	0	0
Lane Group Flow (vph)	0	707	655	0	0	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	0	643	622	0	0	0
Future Vol, veh/h	0	643	622	0	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	91	91	95	95	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	0	707	655	0	0	0
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	655	0	-	0	1362	655
Stage 1	-	-	-	-	655	-
Stage 2	-	-	-	-	707	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	932	-	-	-	163	466
Stage 1	-	-	-	-	517	-
Stage 2	-	-	-	-	489	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	932	-	-	-	163	466
Mov Cap-2 Maneuver	-	-	-	-	163	-
Stage 1	-	-	-	-	517	-
Stage 2	-	-	-	-	489	-
Approach	EB	WB	SB			
HCM Control Delay, s	0	0	0			
HCM LOS			A			
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	932	-	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	-	0	-
HCM Lane LOS	A	-	-	-	A	-
HCM 95th %tile Q(veh)	0	-	-	-	-	-



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	8	337	537	8	7	8
Future Volume (vph)	8	337	537	8	7	8
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr <sub>t</sub>		0.998		0.929		
Fl <sub>t</sub> Protected		0.999		0.977		
Satd. Flow (prot)	0	1985	2107	0	1691	0
Fl <sub>t</sub> Permitted		0.999		0.977		
Satd. Flow (perm)	0	1985	2107	0	1691	0
Adj. Flow (vph)	10	416	603	9	8	9
Lane Group Flow (vph)	0	426	612	0	17	0
Sign Control	Free	Free		Stop		
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0.3					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations		4	1	2		
Traffic Vol, veh/h	8	337	537	8	7	8
Future Vol, veh/h	8	337	537	8	7	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	81	81	89	89	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	10	416	603	9	8	9
Major/Minor						
Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	612	0	-	0	1044	608
Stage 1	-	-	-	-	608	-
Stage 2	-	-	-	-	436	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	967	-	-	-	254	496
Stage 1	-	-	-	-	543	-
Stage 2	-	-	-	-	652	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	967	-	-	-	251	496
Mov Cap-2 Maneuver	-	-	-	-	251	-
Stage 1	-	-	-	-	536	-
Stage 2	-	-	-	-	652	-
Approach						
Approach	EB	WB	SB			
HCM Control Delay, s	0.2	0	16.1			
HCM LOS			C			
Minor Lane/Major Mvmt						
Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	967	-	-	-	341	
HCM Lane V/C Ratio	0.01	-	-	-	0.048	
HCM Control Delay (s)	8.8	0	-	-	16.1	
HCM Lane LOS	A	A	-	-	C	
HCM 95th %tile Q(veh)	0	-	-	-	0.1	



Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	6	654	649	5	5	5
Future Volume (vph)	6	654	649	5	5	5
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr <sub>t</sub>		0.999		0.932		
Fl <sub>t</sub> Protected				0.976		
Satd. Flow (prot)	0	1987	2109	0	1694	0
Fl <sub>t</sub> Permitted				0.976		
Satd. Flow (perm)	0	1987	2109	0	1694	0
Adj. Flow (vph)	7	735	676	5	5	5
Lane Group Flow (vph)	0	742	681	0	10	0
Sign Control		Free	Free		Stop	
Intersection Summary						
Control Type: Unsignalized						

Intersection						
Int Delay, s/veh	0.2					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	6	654	649	5	5	5
Future Vol, veh/h	6	654	649	5	5	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	89	89	96	96	92	92
Heavy Vehicles, %	2	2	2	2	2	2
Mvmt Flow	7	735	676	5	5	5

Major/Minor	Major1	Major2	Minor2			
Conflicting Flow All	681	0	-	0	1428	679
Stage 1	-	-	-	-	679	-
Stage 2	-	-	-	-	749	-
Critical Hdwy	4.12	-	-	-	6.42	6.22
Critical Hdwy Stg 1	-	-	-	-	5.42	-
Critical Hdwy Stg 2	-	-	-	-	5.42	-
Follow-up Hdwy	2.218	-	-	-	3.518	3.318
Pot Cap-1 Maneuver	912	-	-	-	149	452
Stage 1	-	-	-	-	504	-
Stage 2	-	-	-	-	467	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	912	-	-	-	147	452
Mov Cap-2 Maneuver	-	-	-	-	147	-
Stage 1	-	-	-	-	497	-
Stage 2	-	-	-	-	467	-

Approach	EB	WB	SB			
HCM Control Delay, s	0.1	0	22			
HCM LOS			C			

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1	
Capacity (veh/h)	912	-	-	-	222	
HCM Lane V/C Ratio	0.007	-	-	-	0.049	
HCM Control Delay (s)	9	0	-	-	22	
HCM Lane LOS	A	A	-	-	C	
HCM 95th %tile Q(veh)	0	-	-	-	0.2	

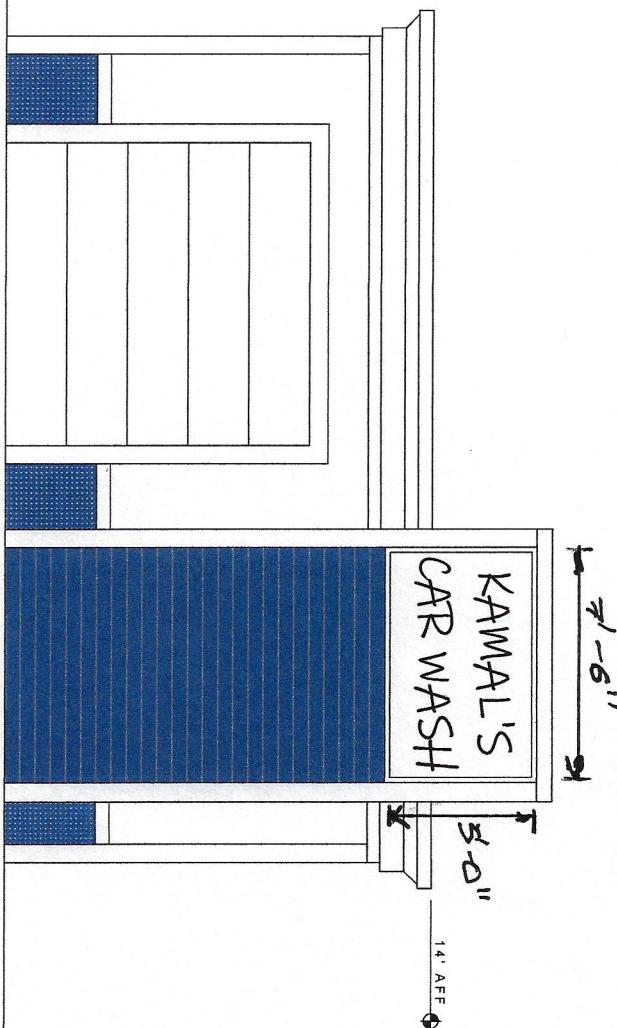


Lane Group	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	12	643	622	11	11	12
Future Volume (vph)	12	643	622	11	11	12
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Fr <sub>t</sub>		0.998			0.930	
Flt Protected		0.999			0.977	
Satd. Flow (prot)	0	1985	2107	0	1693	0
Flt Permitted		0.999			0.977	
Satd. Flow (perm)	0	1985	2107	0	1693	0
Adj. Flow (vph)	13	707	655	12	12	13
Lane Group Flow (vph)	0	720	667	0	25	0
Sign Control		Free	Free		Stop	

Intersection Summary

Control Type: Unsignalized

**SIGN INFORMATION**



SCALE: 1/4" = 1'

#	Revision
1	Draft 8/15/23
2	Draft 8/28/23
3	Draft 11/1/23

KAMAL'S CAR WASH  
METHuen, MA  
ELEVATION

DRAWING NO.	A202
DATE: AUGUST 15, 2023	DRAWN BY: DC
CHECKED BY:	

**STEPHENS-MARQUIS**  
ASSOCIATES, INC.  
777 Daniel Webster Highway  
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Tel: 603-424-2555  
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